

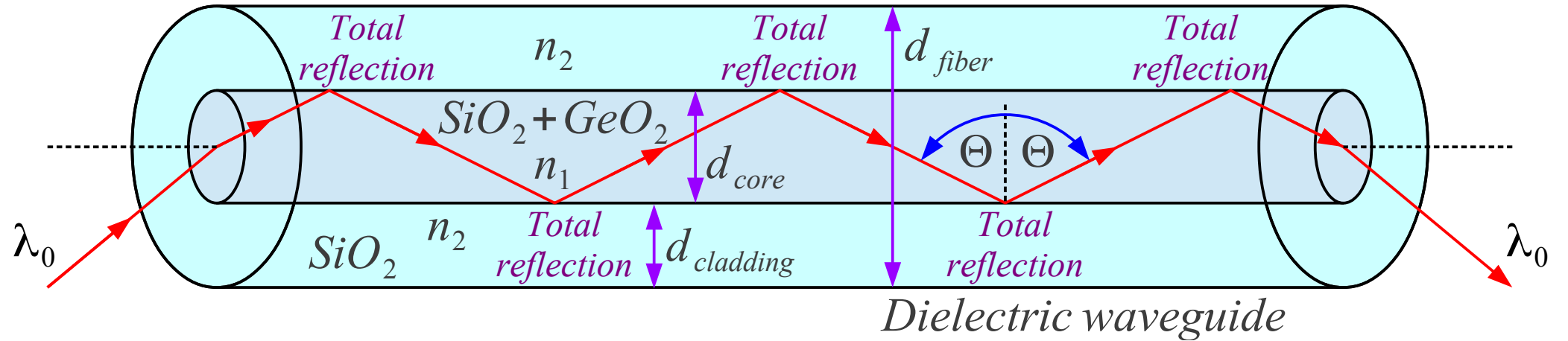
Communication Electronics

Lecture 3:

Optical-fiber communications

Glass optical fiber

Telecom standard: $d_{\text{fiber}} = 125 \mu\text{m}$



Total reflection: $n_1(\text{SiO}_2 + \text{GeO}_2) > n_2(\text{SiO}_2) \rightarrow \arcsin(n_2/n_1) < \Theta < \pi/2$

$$3 \mu\text{m} < d_{\text{core}} < 63 \mu\text{m}$$

$$d_{\text{cladding}} \gg \lambda_0$$

$$780\text{nm} < \lambda_0 < 1630\text{nm} \Leftrightarrow 385\text{THz} > f_0 > 184\text{THz}$$

Advantages in communications:

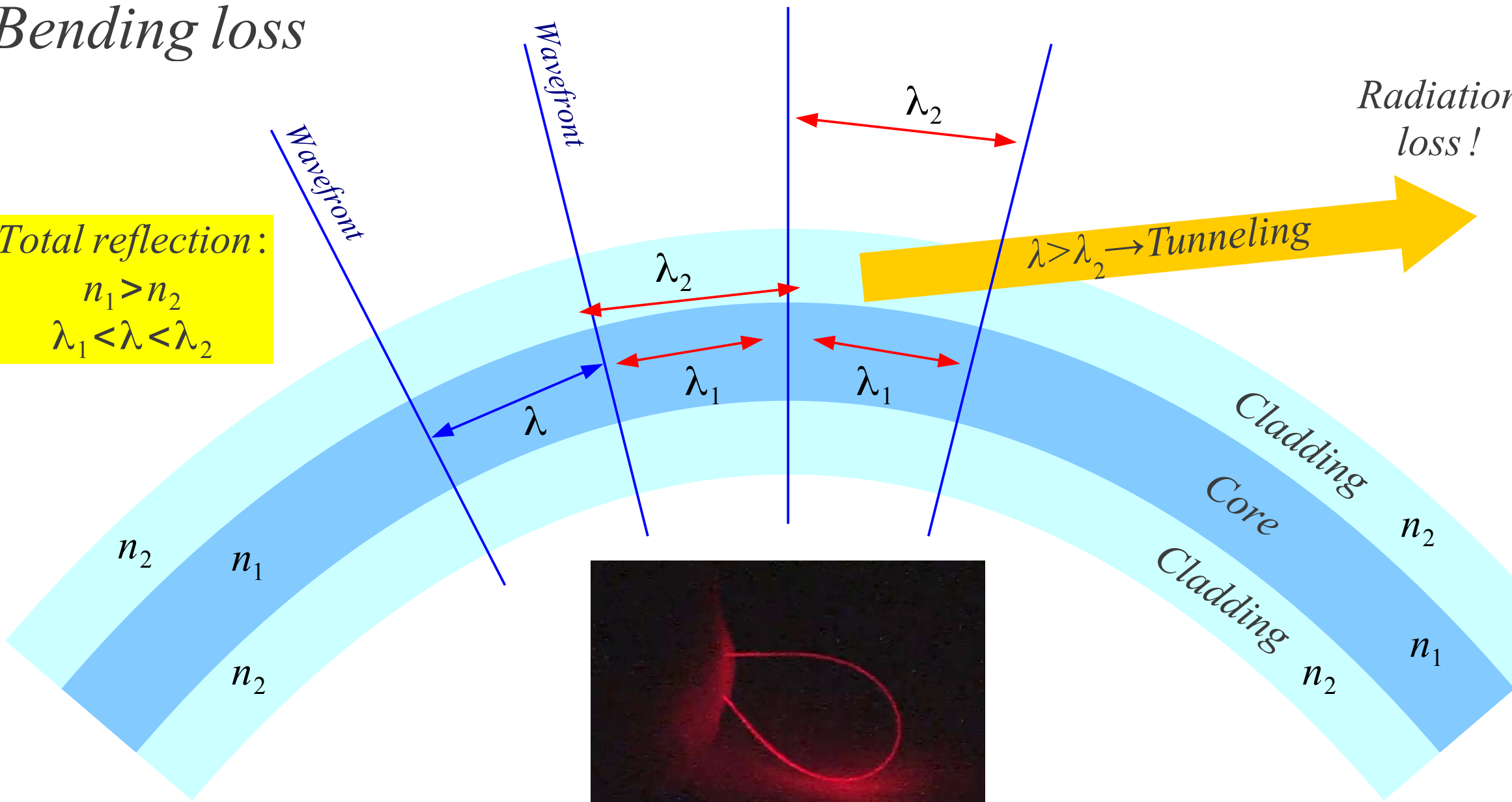
- (1) Low loss: $\alpha/l = -0.15 \dots -2\text{dB/km}$
- (2) Large bandwidth: $B > 4\text{THz}$
- (3) Galvanic isolation!

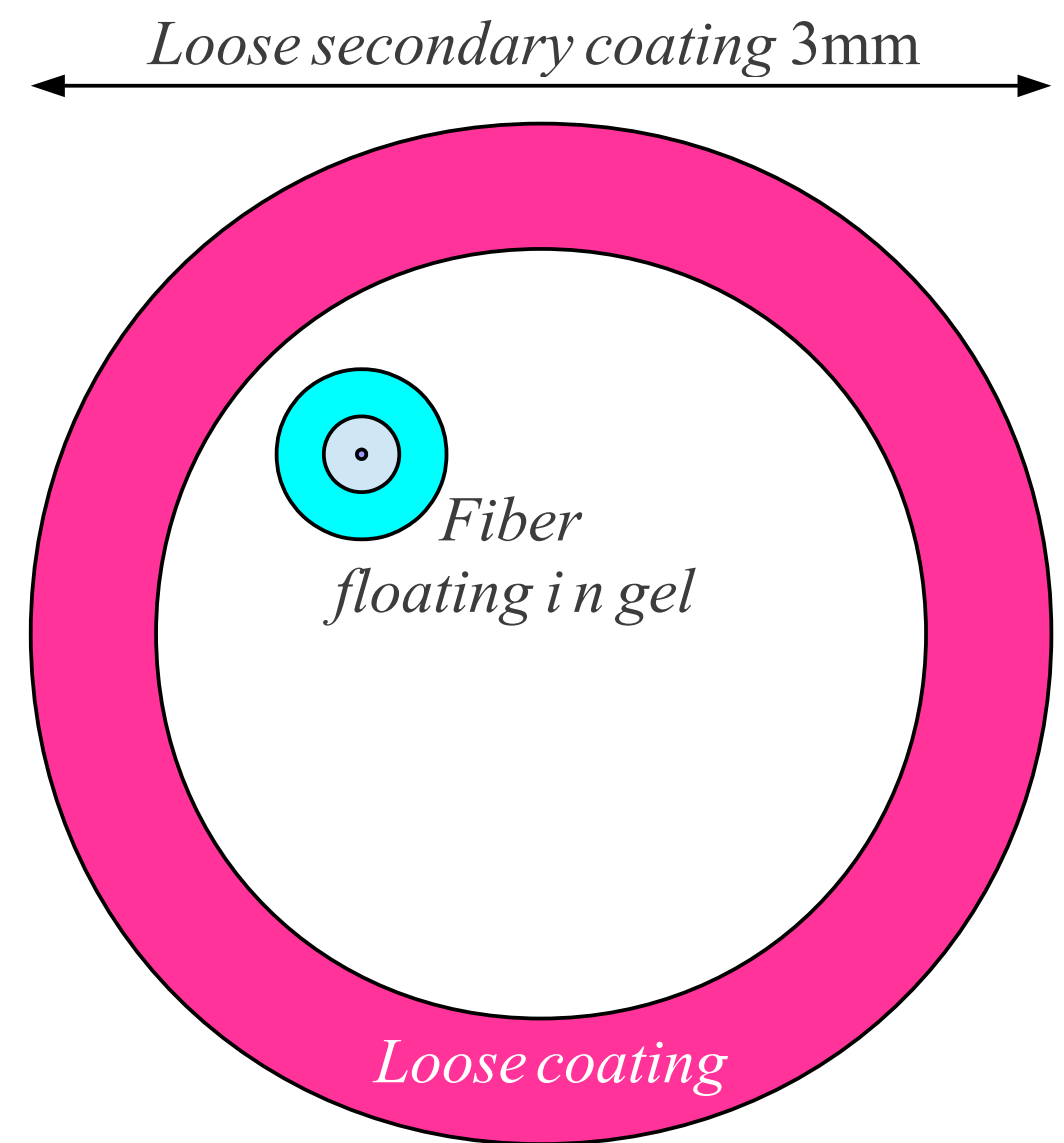
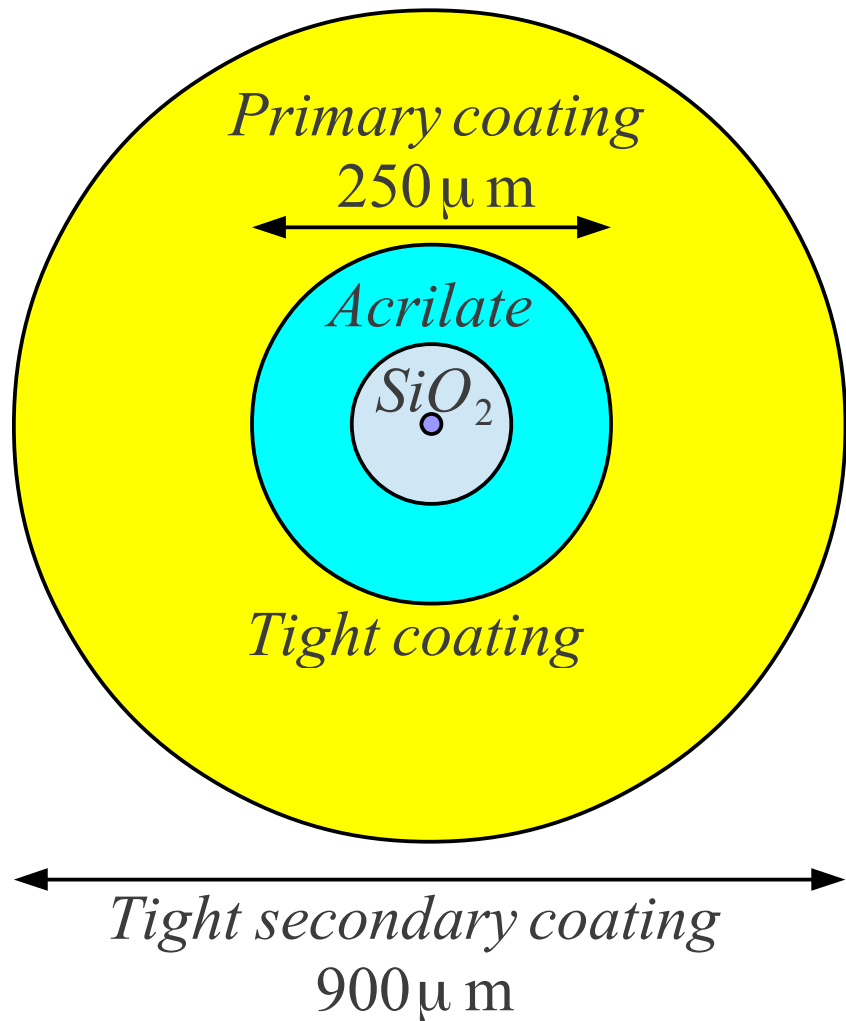
Drawbacks for signal processing:

- (1) Unidirectional amplifier for light-wave frequencies (optical transistor) does not exist!
- (2) Passive components too large for integration!

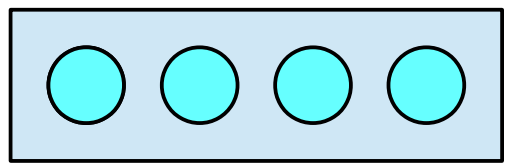
Bending loss

Total reflection:
 $n_1 > n_2$
 $\lambda_1 < \lambda < \lambda_2$

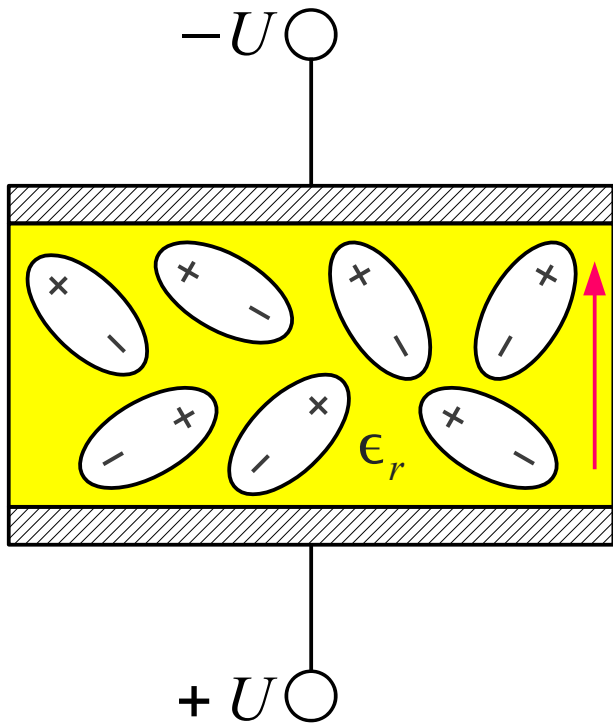




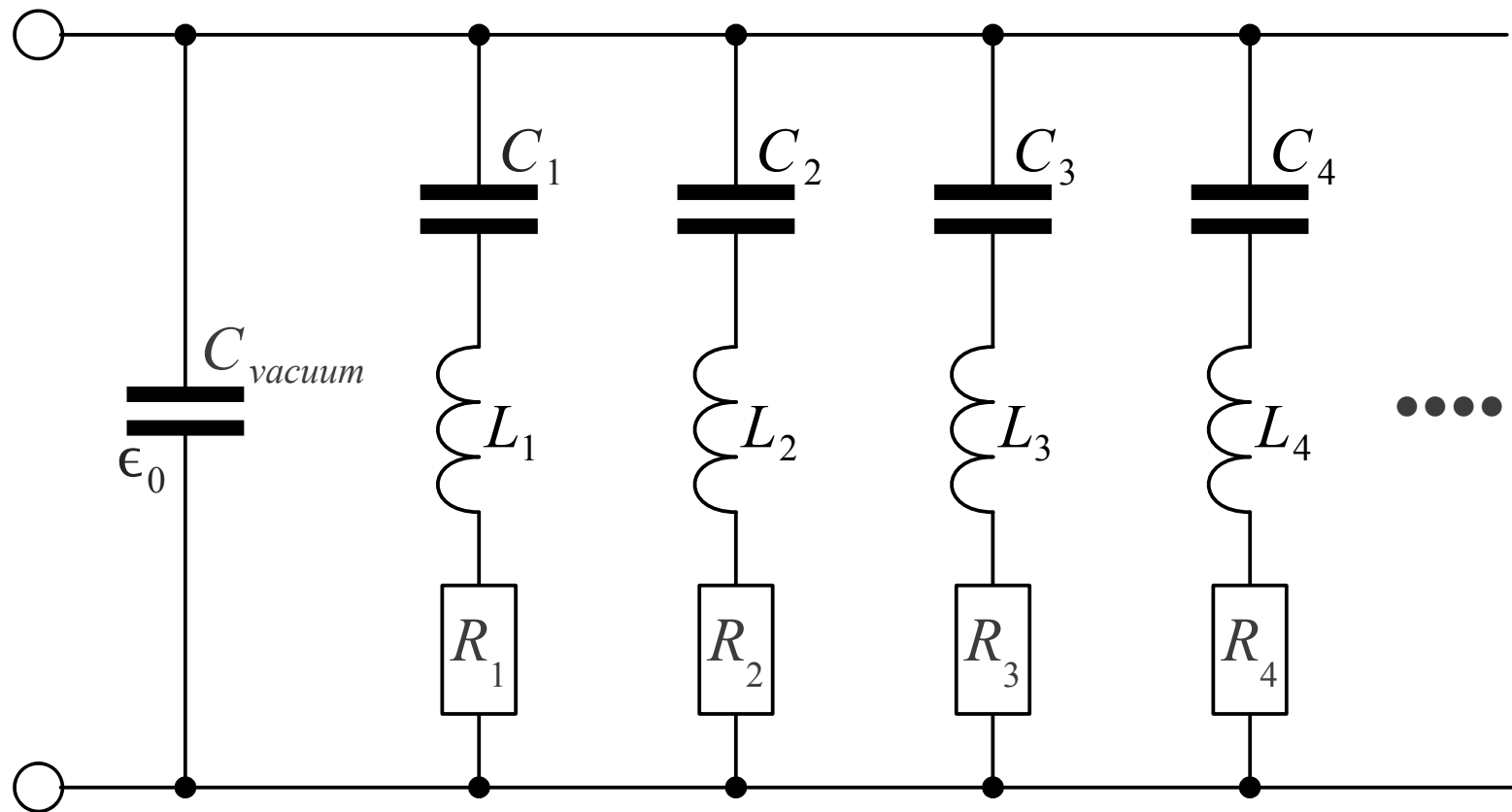
Ribbon 4 ... 24 fibers



Fiber cabling



$$\vec{D} = \epsilon_0 \vec{E} + \vec{P} = \epsilon_0 \epsilon_r \vec{E}$$



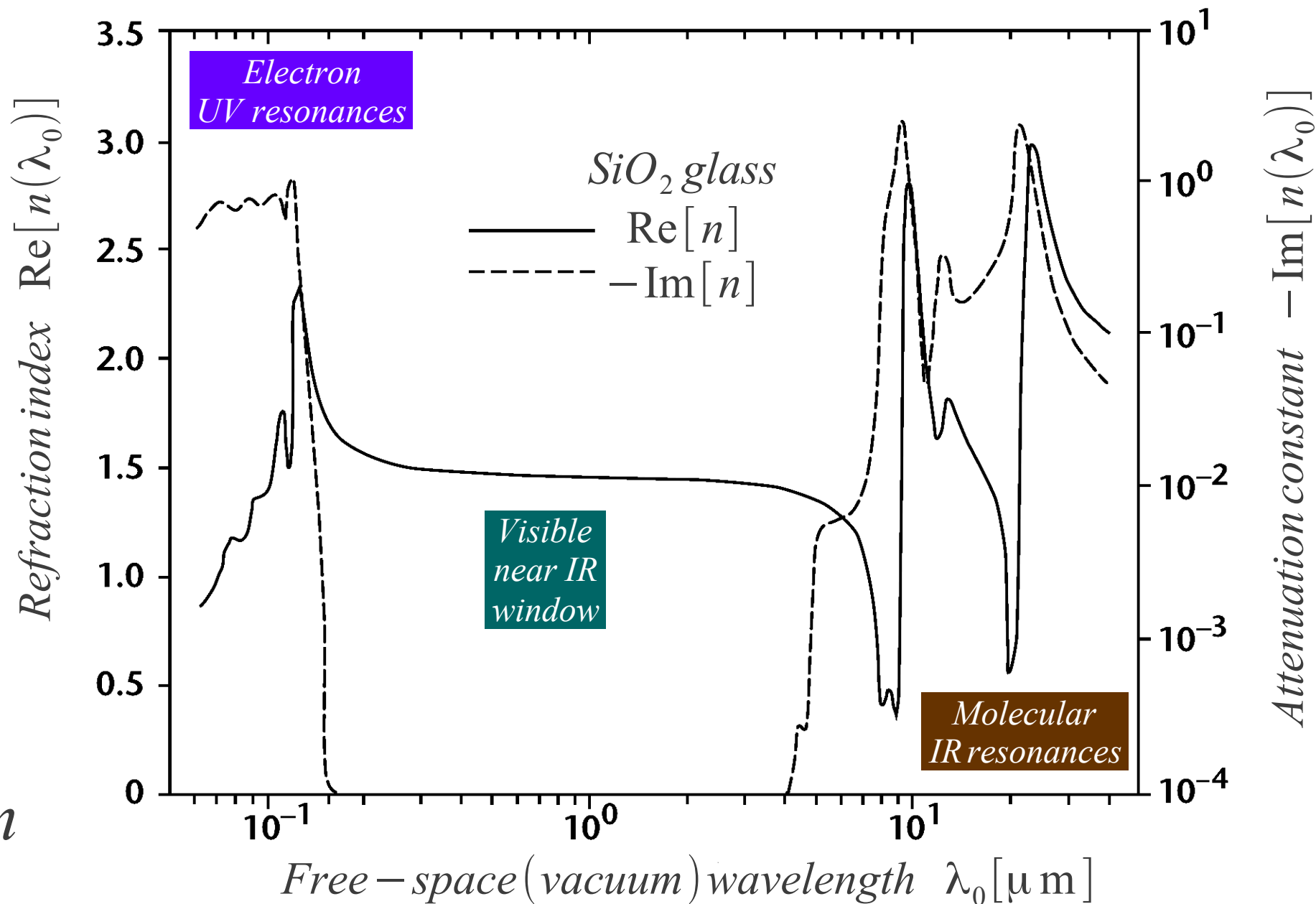
Electron UV resonances $f > 1500\text{THz}$

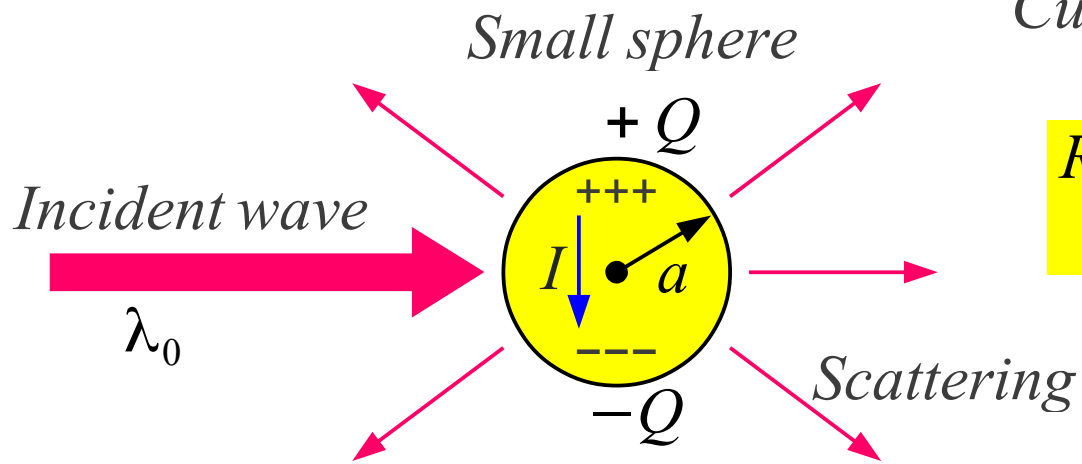
SiO₂ glass

Molecular IR resonances $f < 50\text{THz}$

Equivalent circuit of a dielectric

Complex
refraction
index





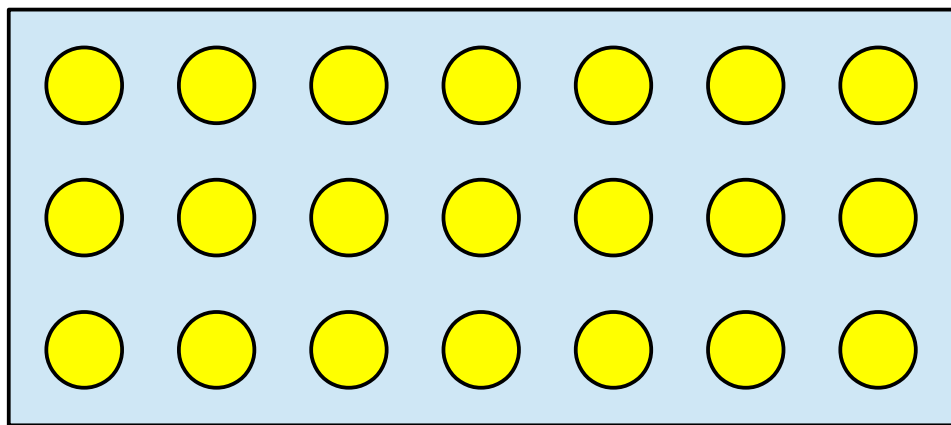
Current / charge continuity: $j \omega Q = I \rightarrow$ radiation!

Rayleigh
 $a \ll \lambda_0$

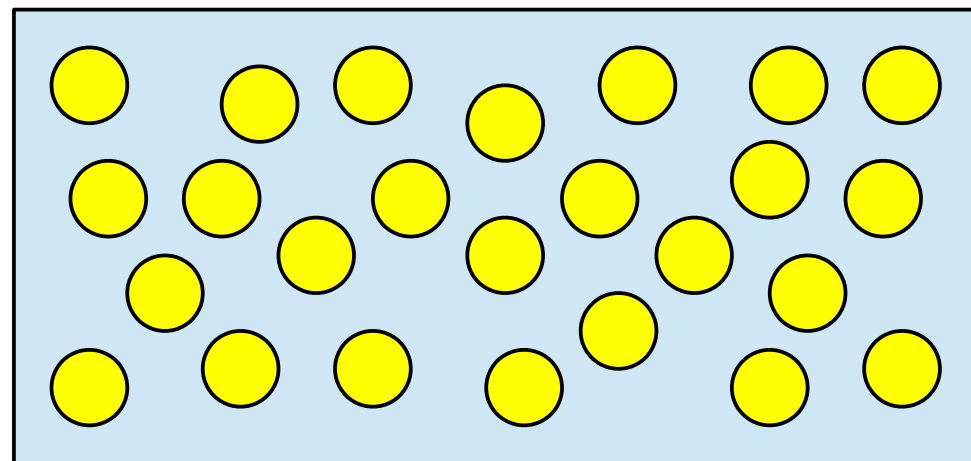
RADAR cross section
of a metal sphere $\sigma = 64 \pi^5 \frac{a^6}{\lambda_0^4}$

RADAR cross section
of a dielectric sphere $\sigma = 64 \pi^5 \frac{a^6}{\lambda_0^4} \left| \frac{\epsilon_r - 1}{\epsilon_r + 2} \right|^2$

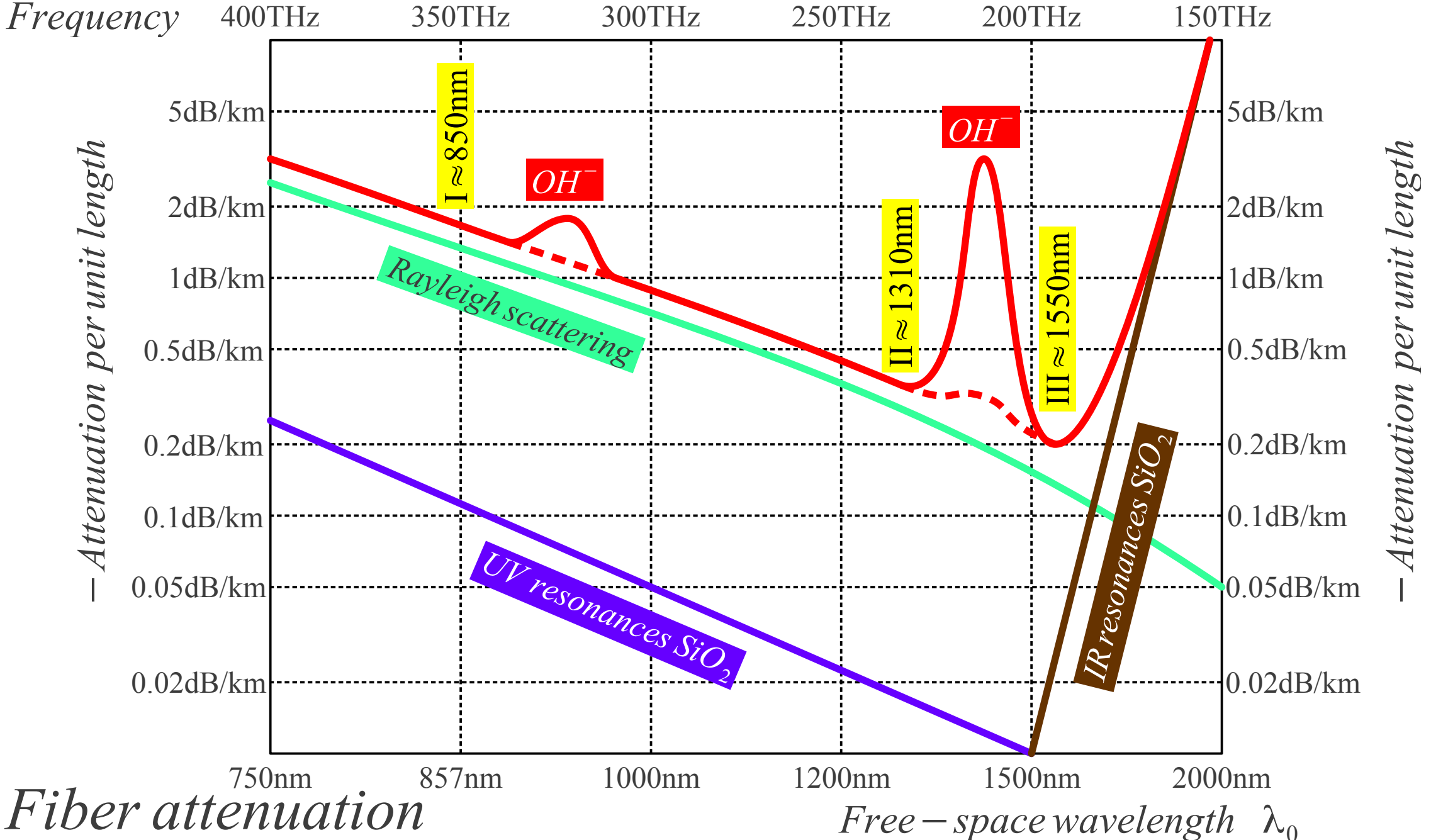
SiO_2 crystal \rightarrow Bragg diffraction

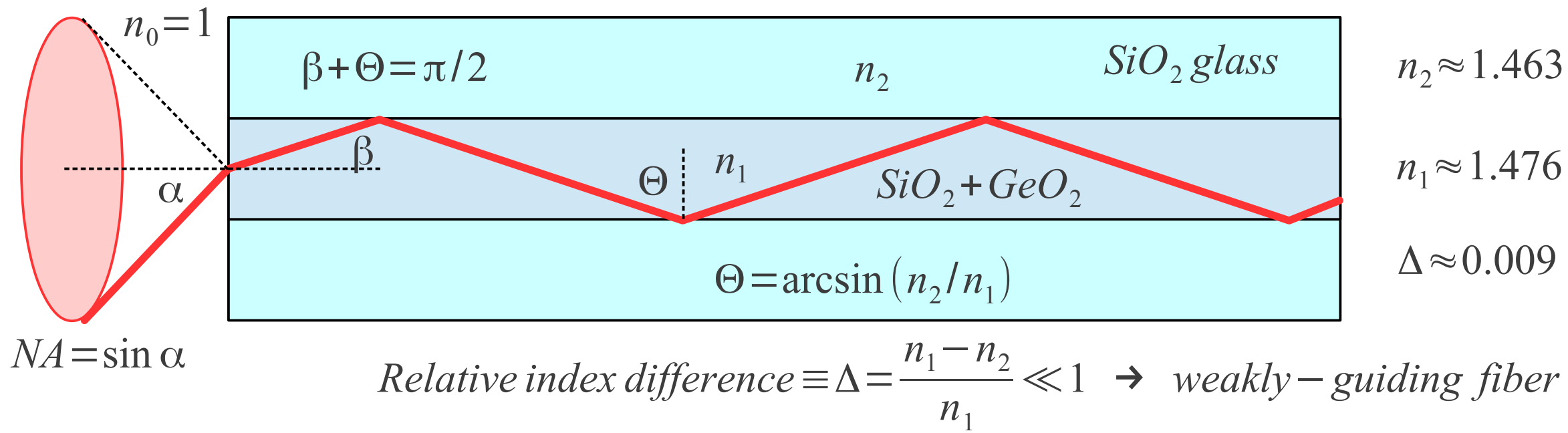


SiO_2 glass \rightarrow Rayleigh scattering

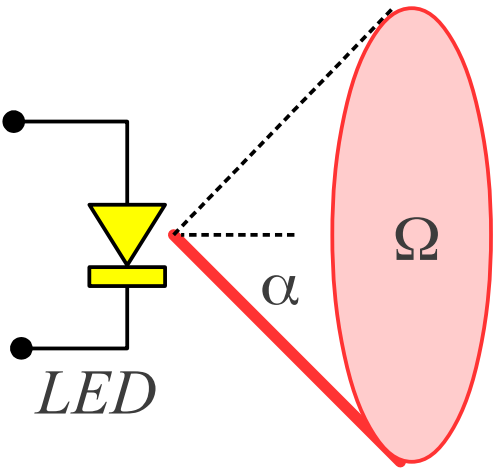


Rayleigh scattering





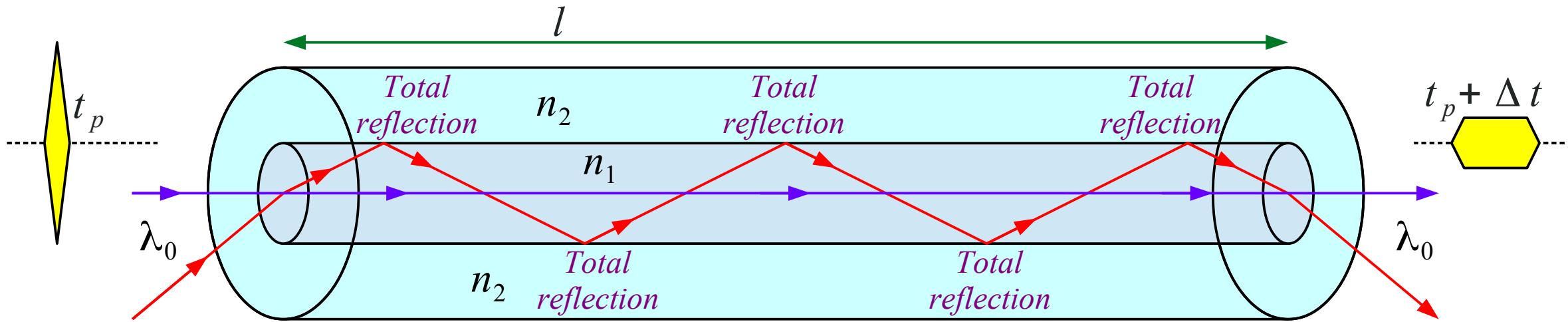
Numerical aperture $\equiv NA = \sin \alpha = \frac{n_1}{n_0} \sin \beta = n_1 \cos \Theta = \sqrt{n_1^2 - n_2^2} \approx n_1 \sqrt{2\Delta} \approx 0.2$



Coupling efficiency $\equiv \eta = \frac{\Omega}{4\pi} = \frac{2\pi(1 - \cos \alpha)}{4\pi} \approx \frac{NA^2}{4} \approx 0.01 = 1\%$

$\cos \alpha = \sqrt{1 - NA^2} \approx 1 - \frac{NA^2}{2}$

Numerical aperture



Straight ray (blue): $t_1 = \frac{n_1 l}{c_0}$

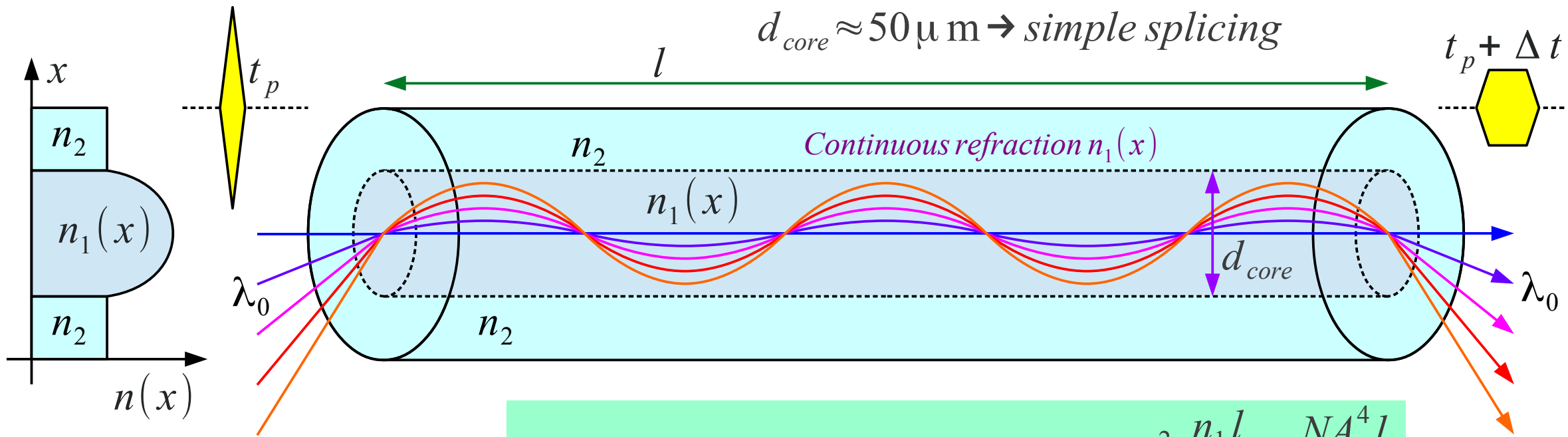
Zigzag ray (red): $t_2 = \frac{n_1 l}{c_0 \sin \Theta_m} = \frac{n_1^2 l}{n_2 c_0}$

Multipath dispersion: $\Delta t = t_2 - t_1 = \frac{n_1 l}{c_0} = \left(\frac{n_1 - n_2}{n_2} \right) \frac{n_1 l}{c_0} \approx \Delta \cdot \frac{n_1 l}{c_0} \approx \frac{NA^2 l}{2 n_1 c_0}$

Example: $NA=0.2 \quad l=10\text{km} \quad n_1=1.47 \rightarrow \Delta t \approx 0.45 \mu\text{s} \rightarrow C \approx \frac{1}{3 \Delta t} \approx 740 \text{ kbit/s}$

Multipath (multimode) dispersion

Useless!



$$NA = \sqrt{n_{1MAX}^2 - n_2^2}$$

$$\text{Multipath dispersion: } \Delta t = t_2 - t_1 \approx \Delta^2 \cdot \frac{n_1 l}{c_0} \approx \frac{NA^4 l}{4 n_1^3 c_0}$$

$$\text{Example: } NA=0.2 \quad l=10\text{km} \quad n_1=1.47 \rightarrow \Delta t \approx 4.2\text{ns} \rightarrow C \approx \frac{1}{3 \Delta t} \approx 80\text{Mbit/s}$$

$$\Delta_{MAX} \approx \frac{NA^2}{2 n_1^2} \approx 0.009$$

Standardized fiber GI 50/125 \equiv ITU G.651

First links ~ 1980 $C \sim 8\text{Mbit/s}$ LED ~ 850nm

Graded index

Use ~ 2020: cheapest SFP modules $C \leq 1\text{Gbit/s}$ @ $l \leq 100\text{m}$

Total reflection: $\Gamma = \frac{a - jb}{a + jb} = e^{j\phi}$

$a_{TE} = \cos \Theta$ $a_{TM} = (n_2/n_1)^2 \cos \Theta$

$b = \pm \sqrt{\sin^2 \Theta - (n_2/n_1)^2}$

$\phi(\Theta) = 2 \arctan(b/a)$ $0 \leq \phi < \pi$

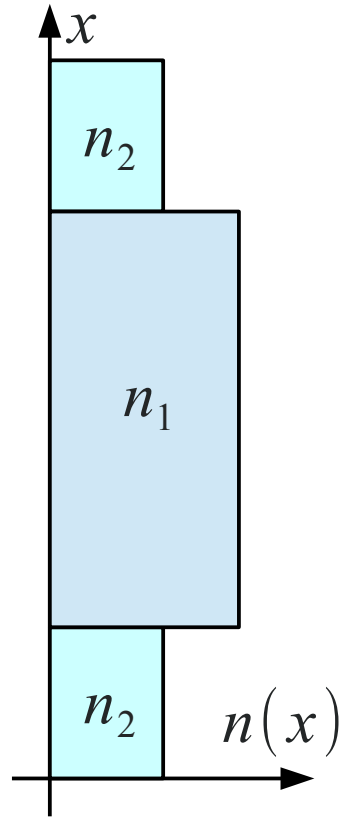
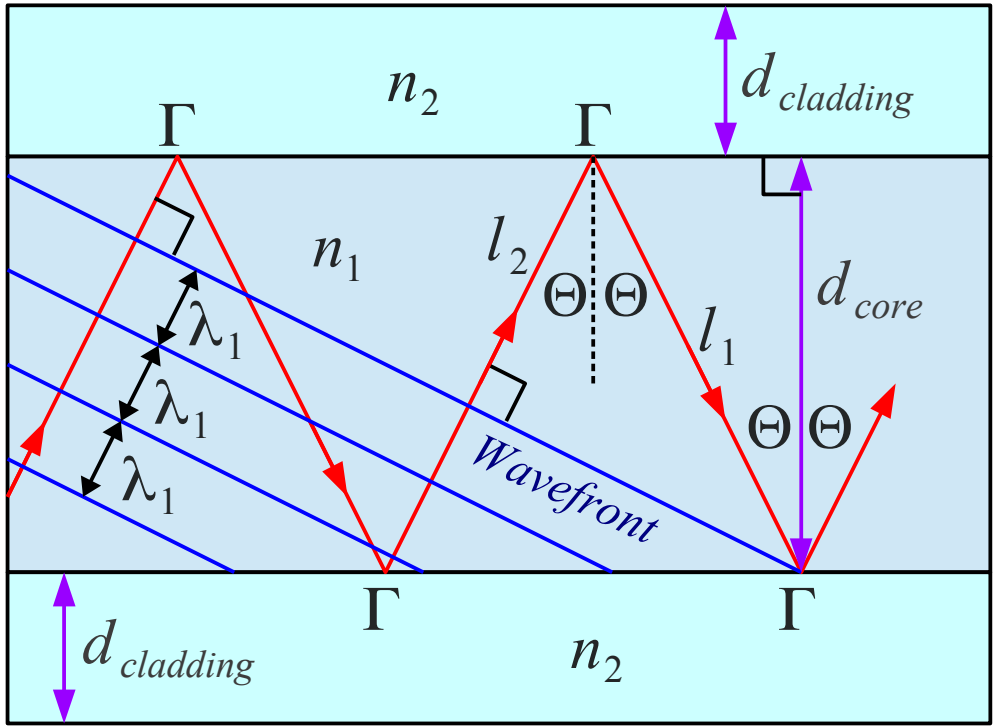
$l_1 = \frac{d_{core}}{\cos \Theta}$ $l_2 = l_1 \cdot \cos 2\Theta$

$l_1 + l_2 = \frac{d_{core}}{\cos \Theta} (1 + \cos 2\Theta) = 2 d_{core} \cos \Theta$

$\lambda_1 = \frac{\lambda_0}{n_1}$ $k_1 = k_0 n_1 = \frac{2\pi}{\lambda_0} n_1 = \frac{\omega}{c_0} n_1$

Transversal phase resonance

Planar 1D waveguide

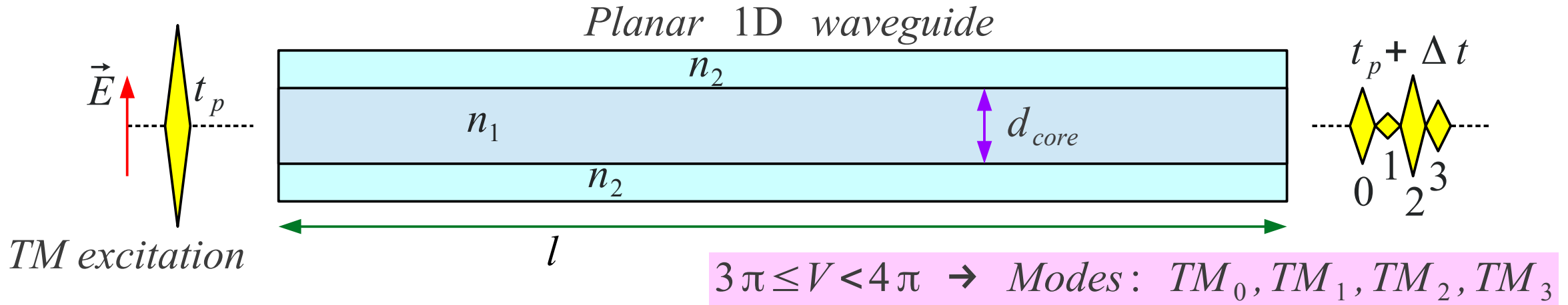


Step-index profile

$(l_1 + l_2) k_1 - 2\phi(\Theta) = m \cdot 2\pi$

$m = 0, 1, 2, 3, 4, 5 \dots \equiv \text{integer}$

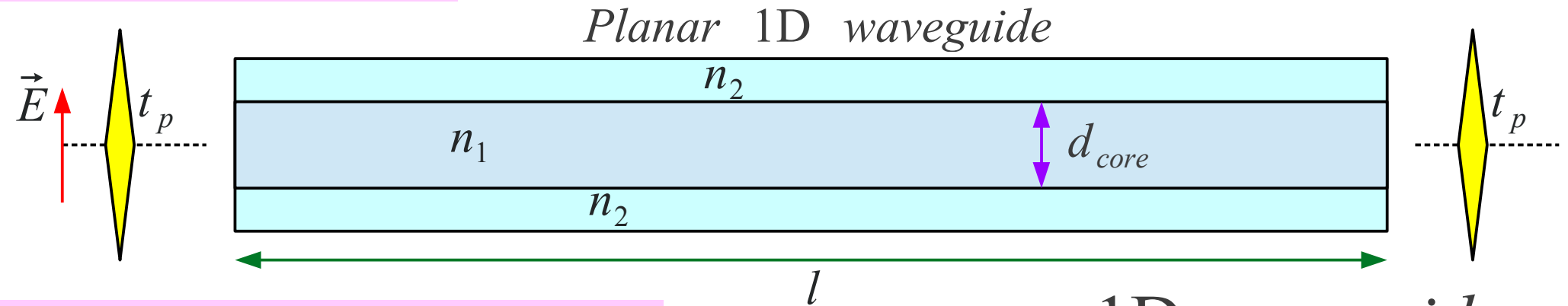
$d_{core} \frac{\omega}{c_0} n_1 \cos \Theta - \phi(\Theta) = m \cdot \pi \rightarrow \Theta = ?$
 TE or TM?



$$0 < n_1 \cos \Theta < n_1 \cos \Theta_m = n_1 \sqrt{1 - \sin^2 \Theta_m} = n_1 \sqrt{1 - (n_2/n_1)^2} = \sqrt{n_1^2 - n_2^2} = NA$$

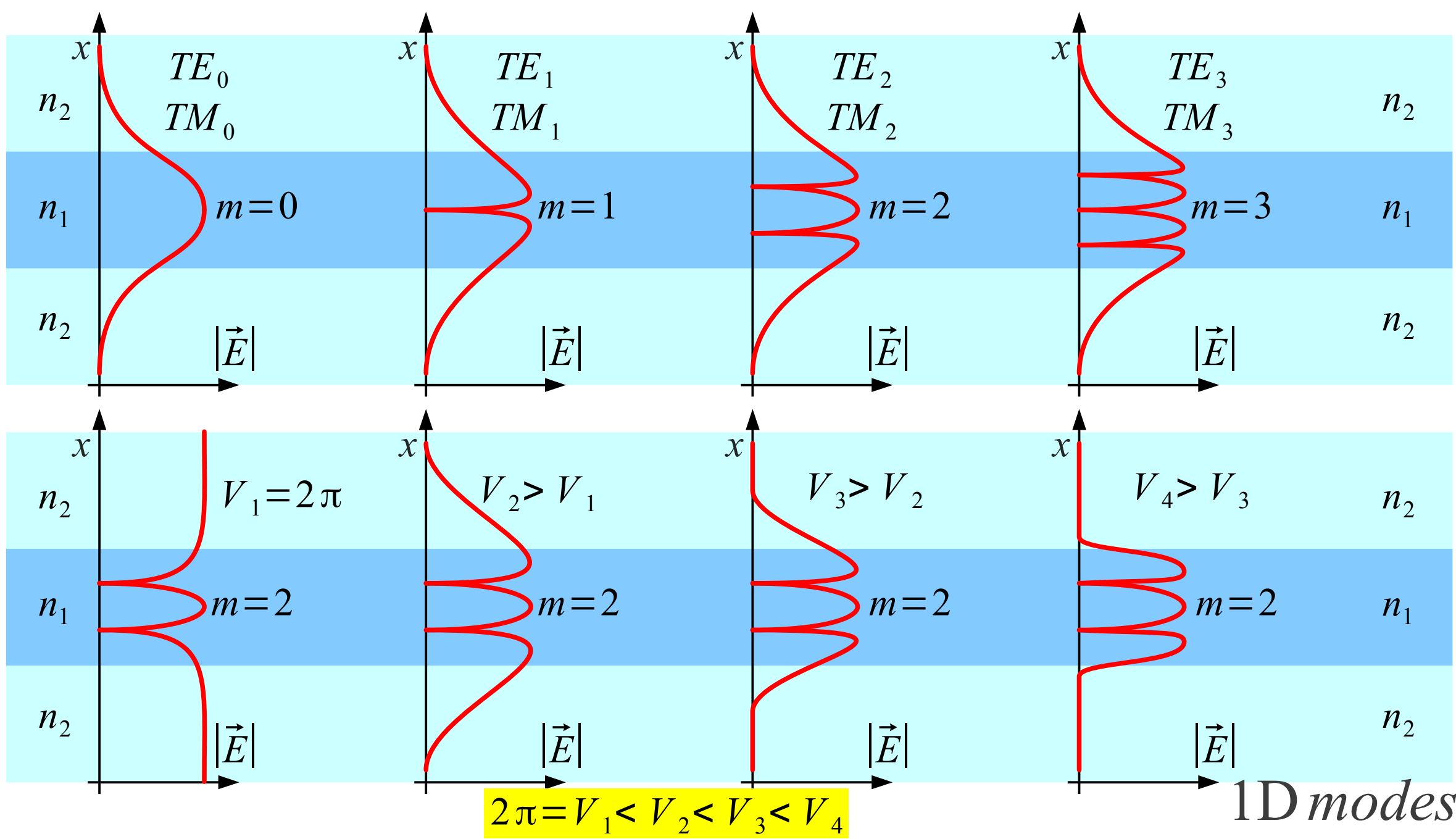
$$\text{Normalized frequency} \equiv V = d_{core} \frac{\omega}{c_0} n_1 \cos \Theta = d_{core} \frac{\omega}{c_0} NA$$

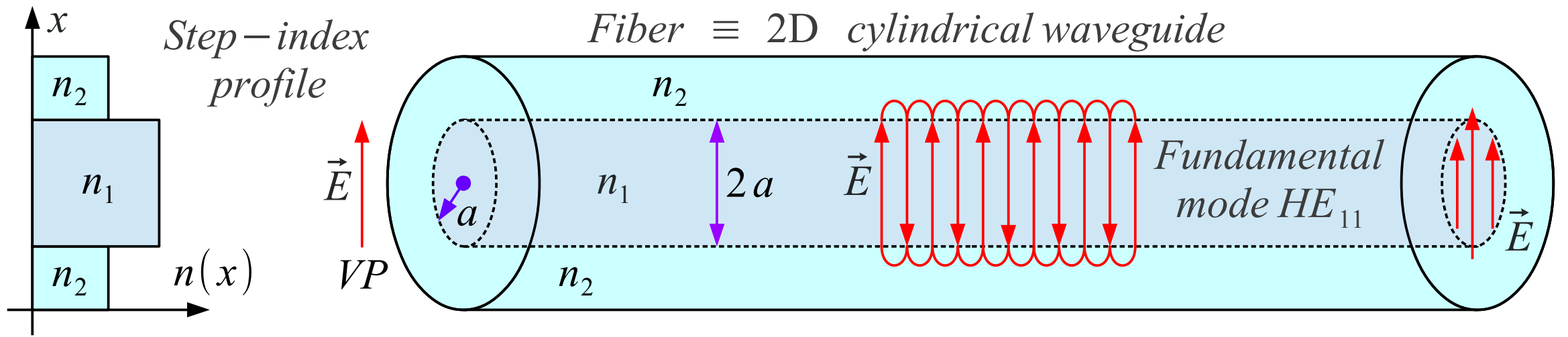
$$0 \leq V < \pi \rightarrow \text{Mode: } TM_0$$



$$V < 1 \rightarrow \text{Field escapes into cladding}$$

1D waveguide modes





Normalized frequency $\equiv V = a \frac{2\pi}{\lambda_0} NA = a \frac{\omega}{c_0} NA$

HE_{11} has two variants HP + VP !

Standardized single-mode fiber
9/125 or 10/125 \equiv ITU G.652*

- $0 \leq V < 2.4049 \rightarrow HE_{11}$ only
- $V < 1.8 \rightarrow$ Field escapes into cladding
- $2.4049 \leq V < 3.8318 \rightarrow$ 4 modes
- $3.8318 \leq V \rightarrow \geq 7$ modes

$2a \approx 9 \dots 10 \mu\text{m}$ $NA \approx 0.1$

$V(1.31 \mu\text{m}) \approx 2.16 \dots 2.40$
 $V(1.55 \mu\text{m}) \approx 1.82 \dots 2.03$

Bessel: $J_0(2.4049) = 0$ $J_1(3.8318) = 0$

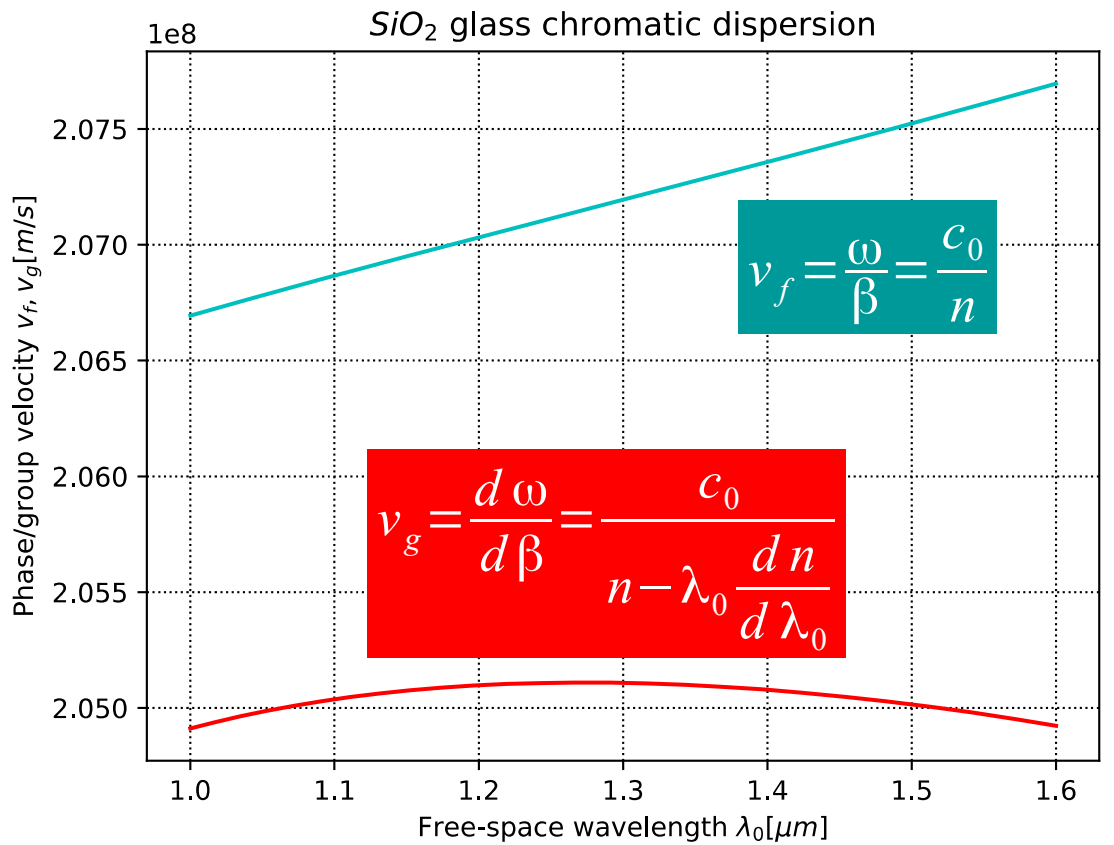
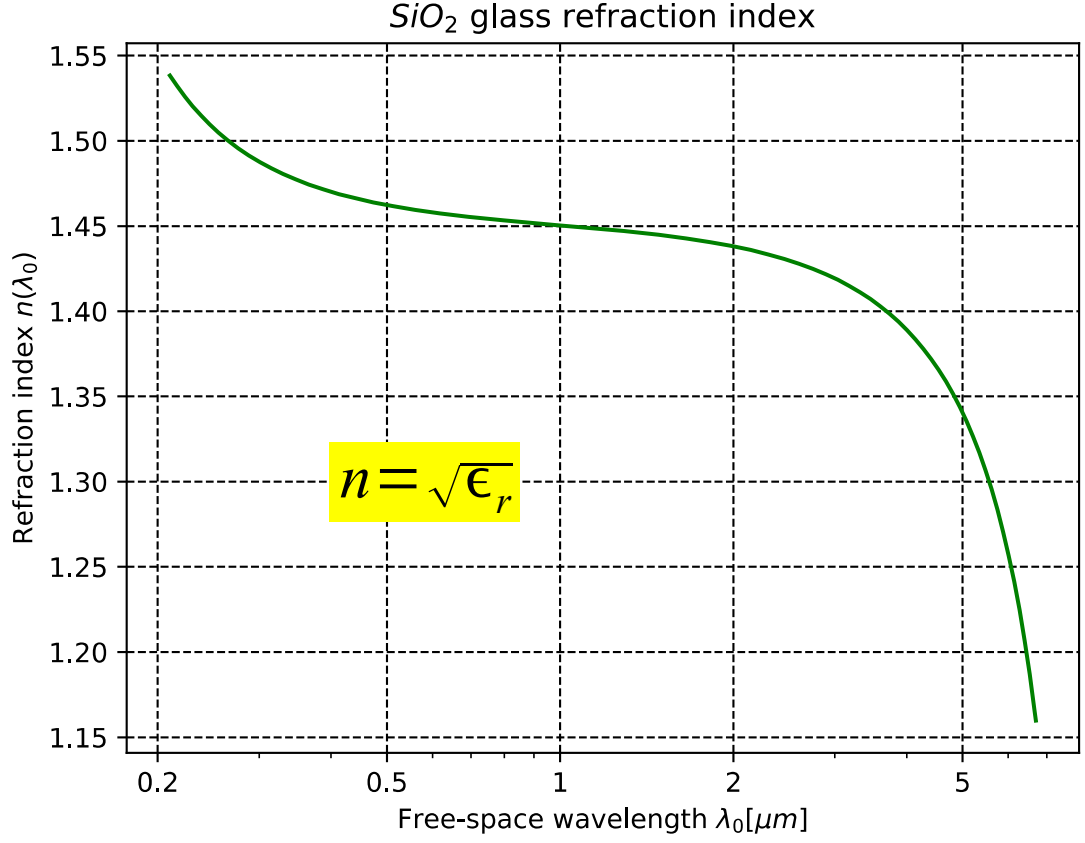
Fiber waveguide modes

G.652* used from 1984
Tolerance tightening*!

Sellmeier for SiO₂ glass $\lambda_0 = 0.21 \dots 6.7 \mu\text{m}$ *Loss-less!*

$$\epsilon_r = 1 + \frac{0.6961663 \cdot \lambda_0^2}{\lambda_0^2 - 0.00467914826} + \frac{0.4079426 \cdot \lambda_0^2}{\lambda_0^2 - 0.0135120631} + \frac{0.8974794 \cdot \lambda_0^2}{\lambda_0^2 - 97.9340025}$$

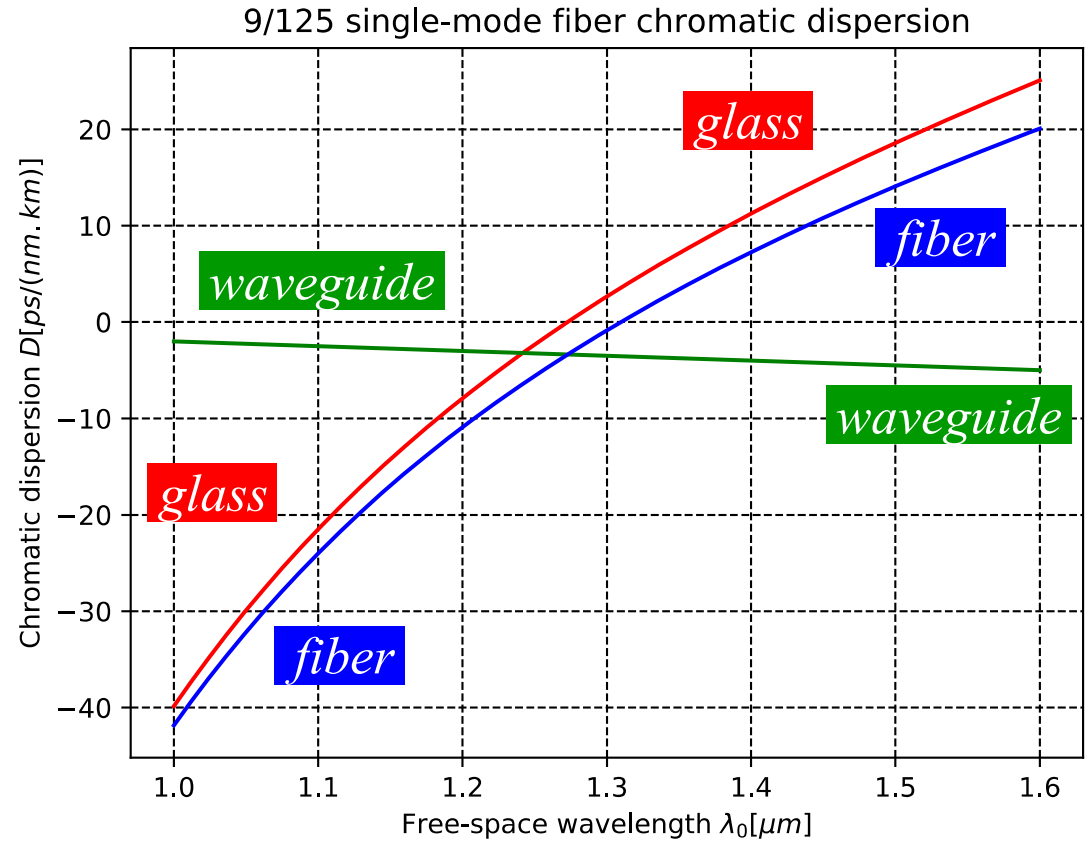
Group velocity v_g slowed down by the reactive power (stored energy) of oscillating SiO₂ electrons / molecules



Speed of light in SiO₂ glass

$$t_g = \frac{l}{v_g} \quad \text{Chromatic dispersion: } \Delta t = D \cdot l \cdot \Delta \lambda_0$$

Group velocity v_g slowed down by the reactive power (stored energy) of
 (1) oscillating SiO_2 electrons/molecules
 (2) waveguide transversal phase resonance



Inexpensive FP laser: $\Delta \lambda_0 = 3\text{nm}$ $l = 50\text{km}$ $C \approx \frac{1}{3 \Delta t}$

$$|D(1.31 \mu\text{m})| < 2 \frac{\text{ps}}{\text{nm} \cdot \text{km}} \rightarrow \Delta t < 300\text{ps} \rightarrow C > 1.1\text{Gbit/s}$$

$$D(1.55 \mu\text{m}) \approx 17 \frac{\text{ps}}{\text{nm} \cdot \text{km}} \rightarrow \Delta t \approx 2.55\text{ns} \rightarrow C \approx 130\text{Mbit/s}$$

$$\text{DFB laser} + \text{LiNbO}_3 \text{ EOM} \rightarrow \frac{1}{\Delta t} \approx C \approx \Delta f = \Delta \lambda_0 \frac{c_0}{\lambda_0^2}$$

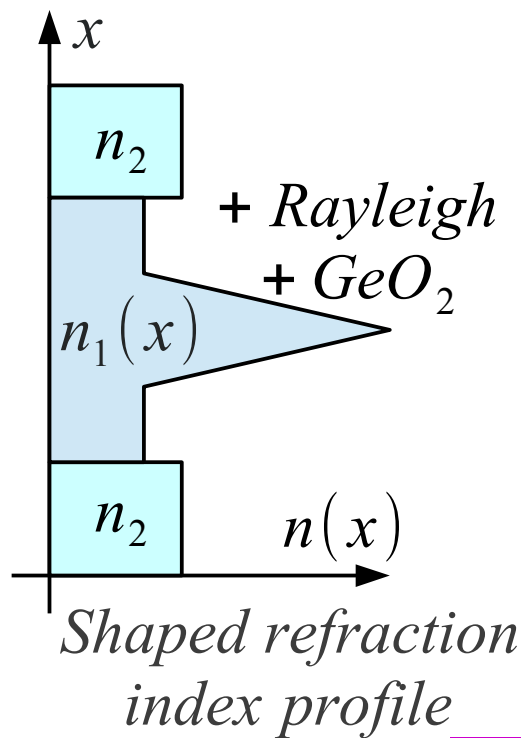
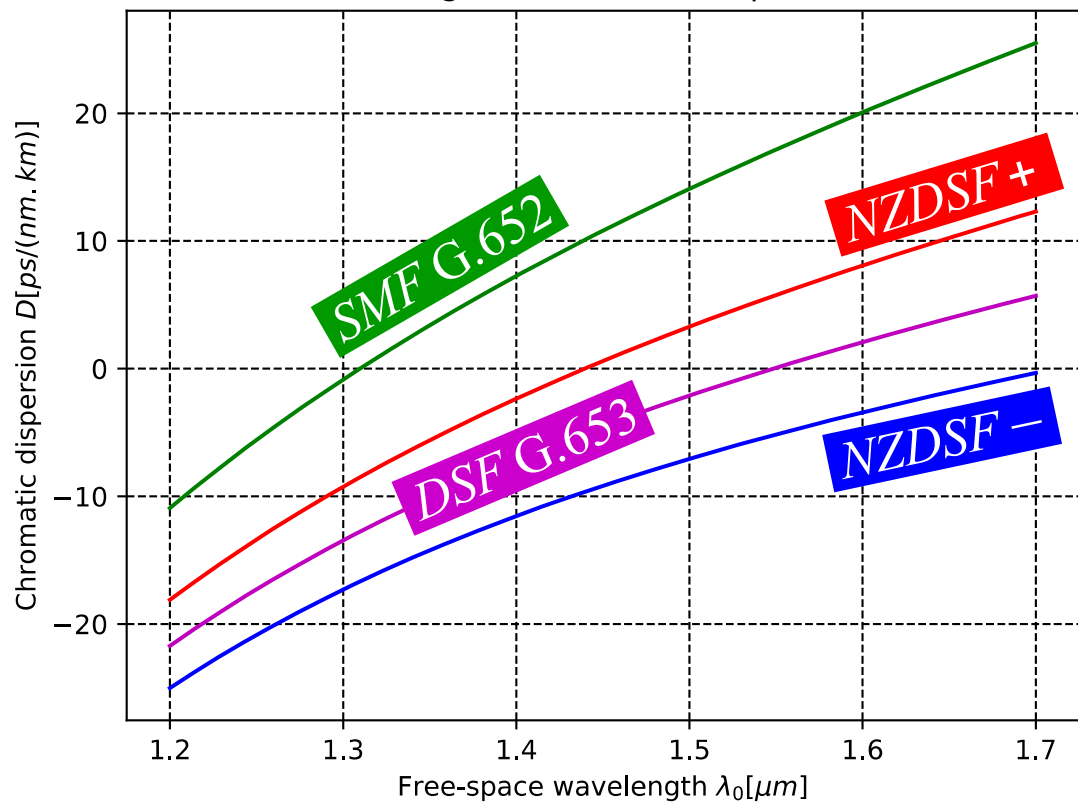
$$l = \frac{\Delta t}{D \cdot \Delta \lambda_0} \approx \frac{c_0}{D \lambda_0^2 C^2} \quad \lambda_0 = 1550\text{nm} \quad D \approx 17 \text{ ps}/(\text{nm} \cdot \text{km})$$

$$D \left[\frac{\text{ps}}{\text{nm} \cdot \text{km}} = 10^{-6} \frac{\text{s}}{\text{m}^2} \right] = \frac{1}{l} \frac{dt_g}{d\lambda_0} = -\frac{1}{v_g^2} \frac{dv_g}{d\lambda_0}$$

Fiber chromatic dispersion

C	2.5Gbit/s	10Gbit/s	40Gbit/s	100Gbit/s
l	1175km	73km	4.59km	0.73km

Shifting the chromatic dispersion



NZDSF \equiv Non – Zero Dispersion – Shifted Fiber

NZDSF+ \equiv ITU G.655
 $D(1550\text{nm}) \approx +4 \dots +7 \frac{\text{ps}}{\text{nm}\cdot\text{km}}$
 $A_{\text{core}} \rightarrow 80 \mu\text{m}^2$ (*LEAF*)

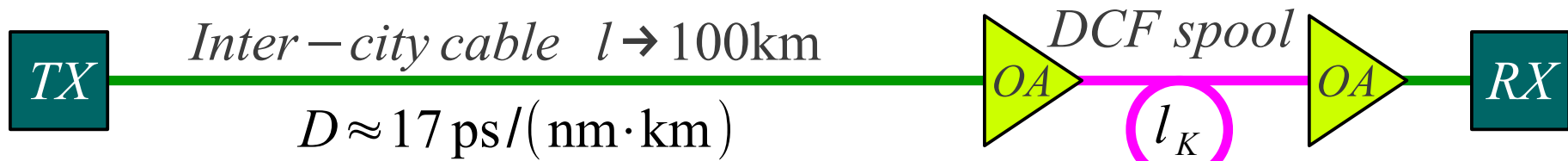
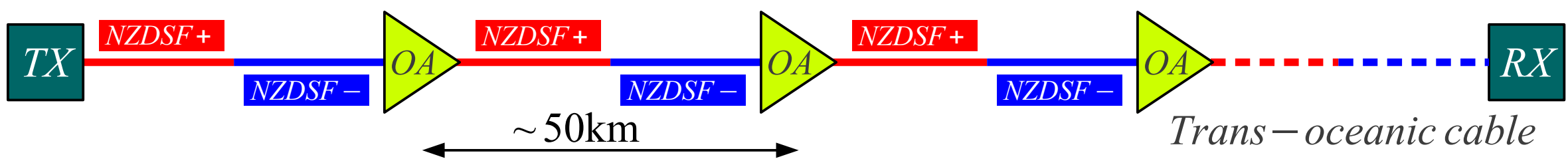
NZDSF-
 $D(1550\text{nm}) \approx -4 \dots -7 \frac{\text{ps}}{\text{nm}\cdot\text{km}}$

DSF (8/125) \equiv ITU G.653
 $D(1550\text{nm}) \approx 0 \frac{\text{ps}}{\text{nm}\cdot\text{km}}$
 $\alpha/l \approx 0.5\text{dB}/\text{km} \rightarrow 0.25\text{dB}/\text{km}$
 $A_{\text{core}} \approx 30 \mu\text{m}^2$
Useless due to nonlinearity

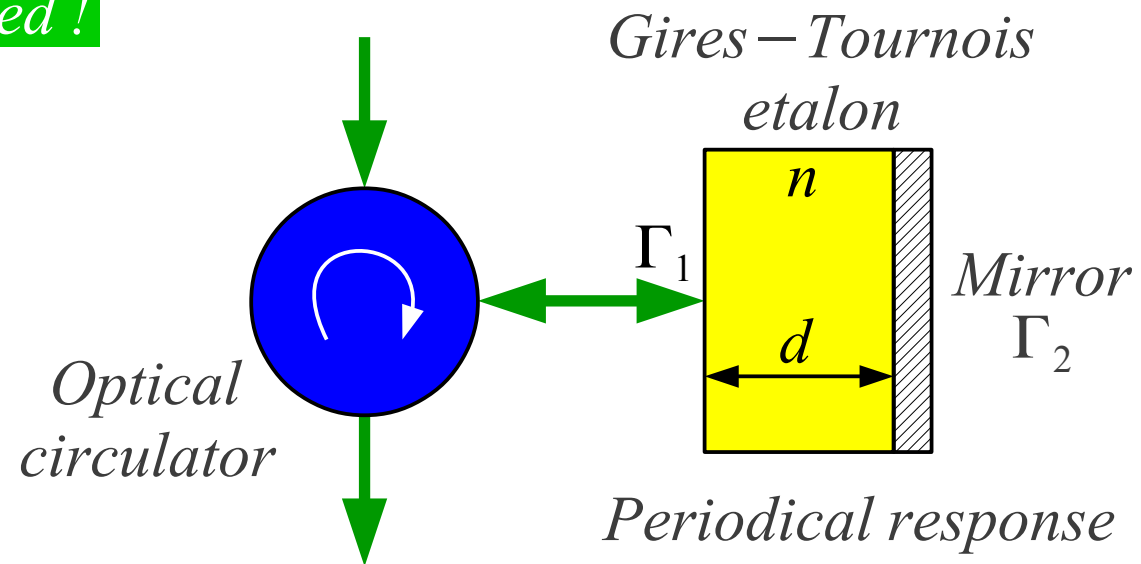
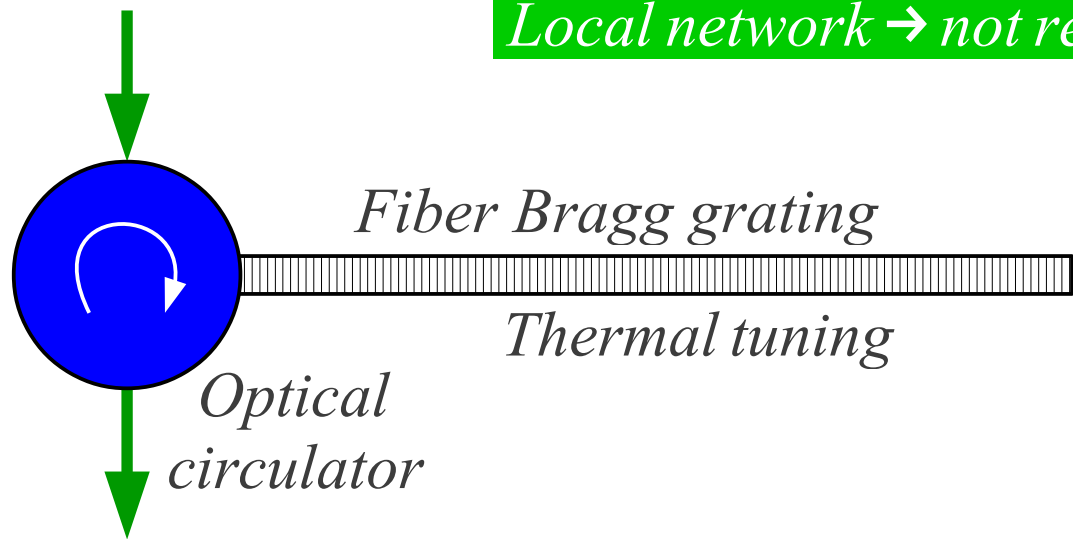
9/125 (10/125) \equiv ITU G.652
 $D(1550\text{nm}) \approx +17 \frac{\text{ps}}{\text{nm}\cdot\text{km}}$
 $\alpha/l \approx 0.2\text{dB}/\text{km} \rightarrow 0.15\text{dB}/\text{km}$
 $A_{\text{core}} \approx 70 \mu\text{m}^2$

Dispersion – compensating fiber
 $D(1550\text{nm}) \approx -80 \frac{\text{ps}}{\text{nm}\cdot\text{km}}$
 $\alpha/l \approx 1\text{dB}/\text{km}$

Dispersion – shifted fibers

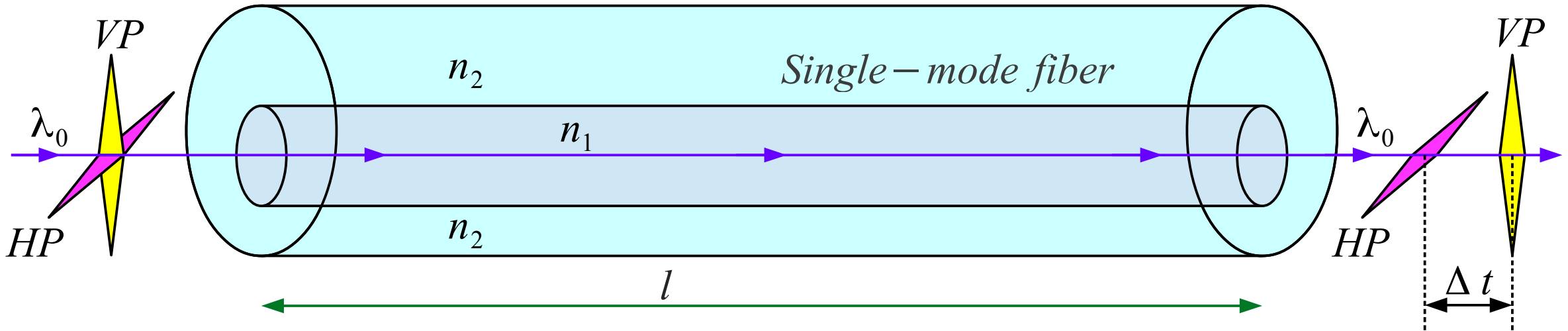


Local network → not required !



Chromatic-dispersion compensation

Eccentric core → Mechanical forces → Birefringence → PMD



HE_{11} has two variants HP + VP, that are not perfectly identical (manufacturing tolerances!)

$PMD \equiv$ Polarization Mode Dispersion

*Birefringence is distributed randomly!
Optical fiber does not maintain polarization!*

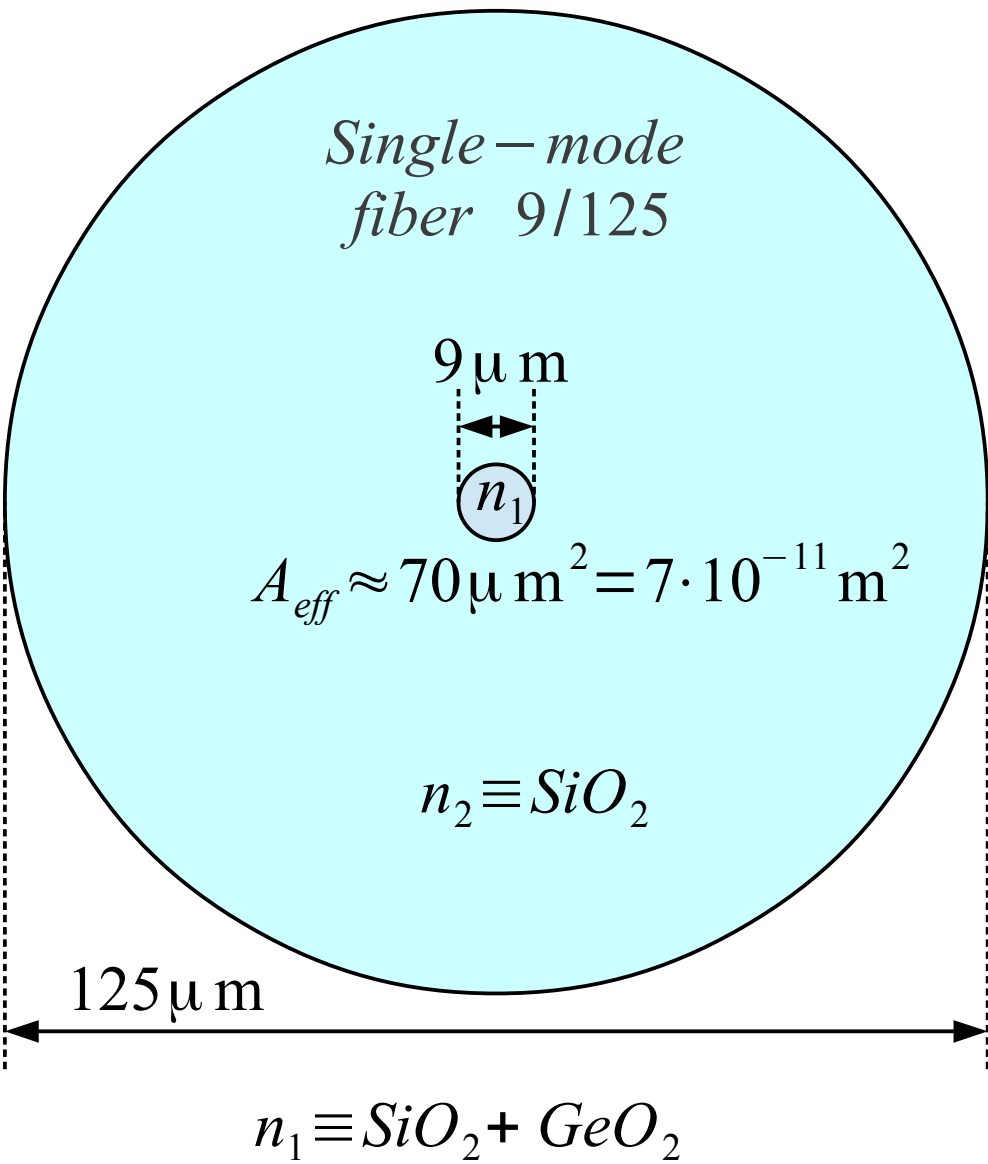
$\Delta t \approx D_{PMD} \cdot \sqrt{l} \quad @ \quad l > 1\text{km}$

	D_{PMD}	$\Delta t(100\text{km})$	$\Delta t(10000\text{km})$
Old fibers <2000	$\sim 10\text{ps}/\sqrt{\text{km}}$	$\sim 100\text{ps}$	$\sim 1\text{ns}$
Spun fibers >2000	$\sim 0.1\text{ps}/\sqrt{\text{km}}$	$\sim 1\text{ps}$	$\sim 10\text{ps}$

*$\Delta t \equiv$ random!
Installed cable
changing slowly:
weeks, months...*

Spinning during fiber drawing ~ 5 turns/m

PMD



Example: $P \approx 100\text{mW}$ $n_1 \approx 1.46$ $Z_0 \approx 377 \Omega$

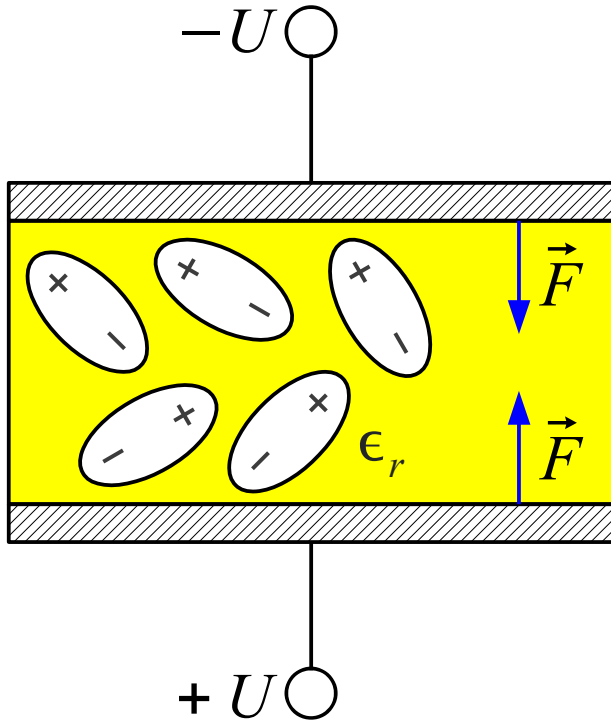
$$S = \frac{P}{A_{\text{eff}}} \approx \frac{100\text{mW}}{7 \cdot 10^{-11} \text{m}^2} \approx 1.4\text{GW}/\text{m}^2 = 140\text{kW}/\text{cm}^2$$

$$|\vec{E}| = \sqrt{\frac{2Z_0 S}{n_1}} \approx 850\text{kV}/\text{m} = 8.5\text{kV}/\text{cm}$$

P	Effect
1mW	Nonlinear response!
10mW	Connector burn-out!
100mW	Max P for connectors!
1W	Max P in fiber!
10W	Fiber-core melting!

Fiber – material loading

Electrostriction \rightarrow increase $n = \sqrt{\epsilon_r} \uparrow$



$$n(E) = n_0 + n_1' \cdot E + n_2' \cdot E^2 + n_3' \cdot E^3 + \dots$$

$n_2' \equiv$ Kerr effect (*electrostriction*)

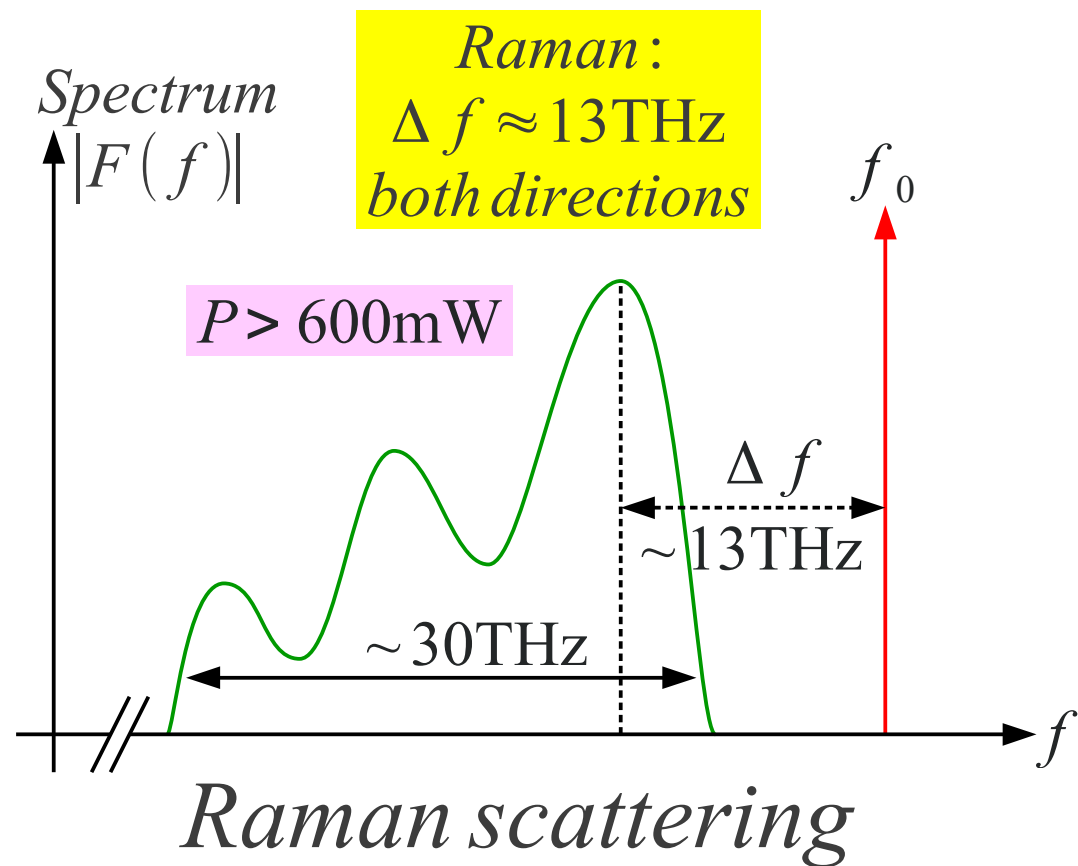
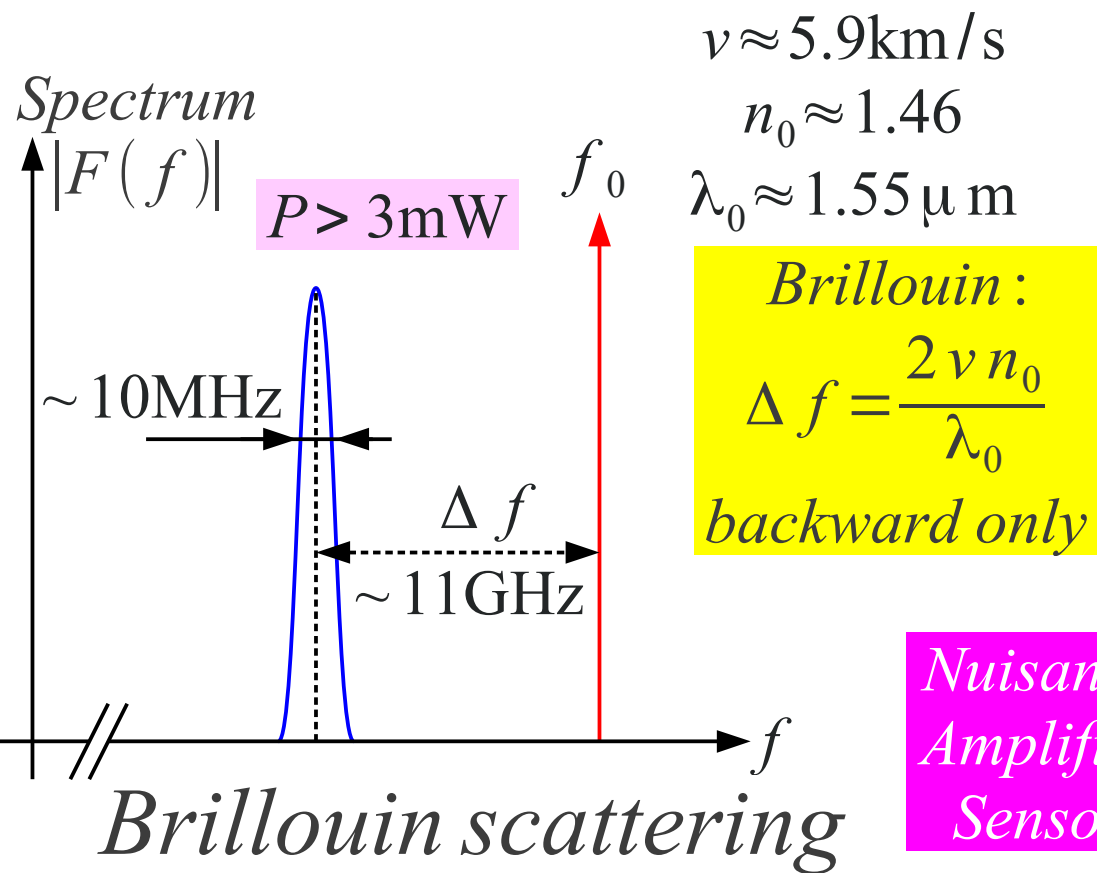
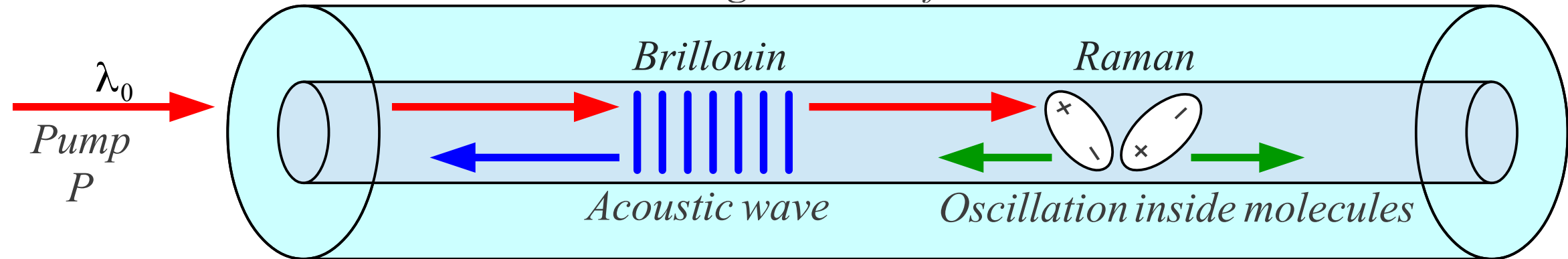
$n_1' \equiv$ Pockels effect (*electrostriction + internal E_0*)

$\text{SiO}_2(+\text{GeO}_2)$ glass \rightarrow internal $E_0 = 0 \rightarrow n_1' = 0$

$$S = \frac{E^2}{2Z} \rightarrow n(S) = n_0 + n_2 \cdot S$$

$$\text{SiO}_2(+\text{GeO}_2) \text{ glass: } n_0 \approx 1.46 \quad n_2 \approx 2.5 \cdot 10^{-20} \frac{\text{m}^2}{\text{W}} \dots 3.2 \cdot 10^{-20} \frac{\text{m}^2}{\text{W}}$$

Electrostriction in glass



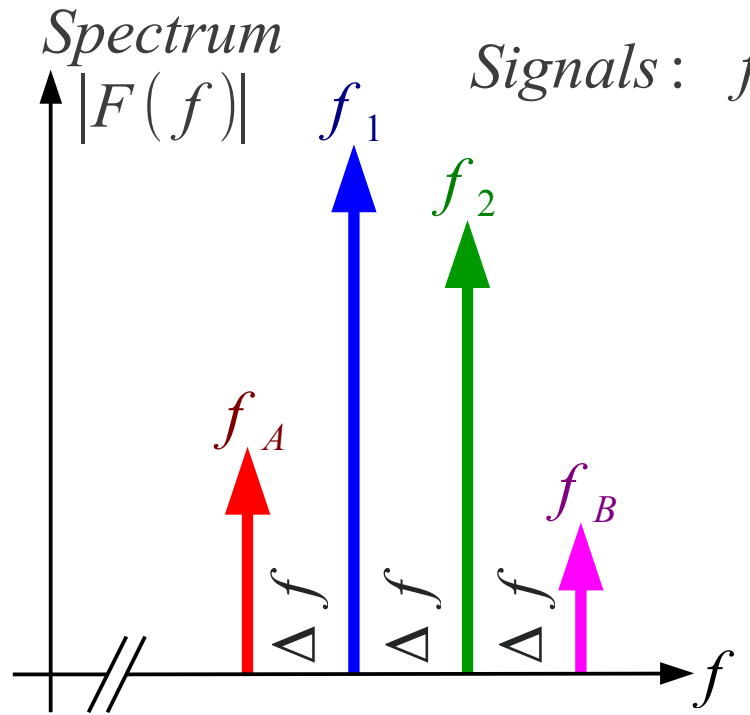
Self phase modulation: $\Delta\phi = \Delta k \cdot l = \frac{2\pi n_2 P}{\lambda_0 A_{eff}} \cdot l \approx 0.15 \text{rd}$

$P = 100 \text{mW}$ $A_{eff} = 70 \mu \text{m}^2$
 $n_2 \approx 2.5 \cdot 10^{-20} \text{m}^2/\text{W}$
 $\lambda_0 = 1550 \text{nm}$ $l = 1 \text{km}$

Linear D – Nonlinear n → Soliton transmission ~ 1995?

Cross phase modulation → Four – Wave Mixing (FWM)

Radio engineers 50 years earlier than optics : Inter – Modulation Distortion (IMD)



Signals: f_1 f_2 → Mixing products: $f_A = 2f_1 - f_2$ $f_B = 2f_2 - f_1$

$P_A = \frac{P_1^2 P_2}{P_{IP3}^2}$

$P_{IP3} [\text{W}] = \frac{\lambda_0 A_{eff}}{2\pi n_2 l_{eff}}$

$\alpha \left[\frac{\text{Np}}{\text{m}} \right] = \frac{-\ln 10}{20} a/l \left[\frac{\text{dB}}{\text{m}} \right]$

$P_B = \frac{P_1 P_2^2}{P_{IP3}^2}$

Long fiber: $l \gg l_{eff} [\text{m}] = \frac{1}{\sqrt{(2\alpha)^2 + (\Delta\beta)^2}}$

Four – Wave Mixing

Phase mismatch: $\Delta\beta \left[\frac{\text{rd}}{\text{m}} \right] = \beta_2 + \beta_A - 2\beta_1 \approx -\frac{2\pi\lambda_0^2 D}{c_0} \cdot (\Delta f)^2$

~ 1995 → DSF G.653

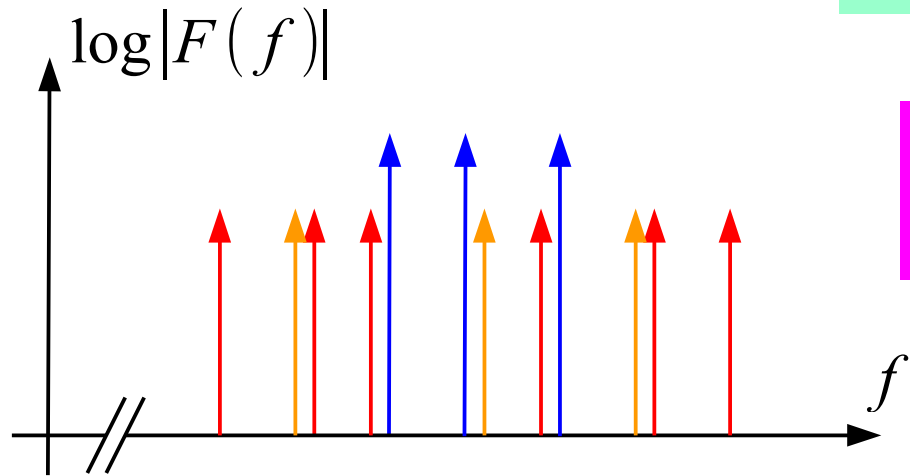
$$a/l \approx -0.3 \text{ dB/km} \quad A_{\text{eff}} \approx 30 \mu\text{m}^2$$

$$D \approx 0 \rightarrow \Delta\beta \approx 0$$

$$l_{\text{eff}} \approx \frac{1}{2\alpha} \approx 14.5 \text{ km}$$

$$P_{\text{IP3}} \approx 20 \text{ mW} = +13 \text{ dBm}$$

$$\lambda_0 \approx 1550 \text{ nm}$$
$$n_2 = 2.5 \cdot 10^{-20} \frac{\text{m}^2}{\text{W}}$$
$$B \approx 4 \text{ THz}$$



4 channels WDM × 2.5 Gb/s = 10 Gb/s

Trans-oceanic cable

~ 2015 → NZDSF G.655

$$a/l \approx -0.2 \text{ dB/km} \quad A_{\text{eff}} \approx 80 \mu\text{m}^2$$

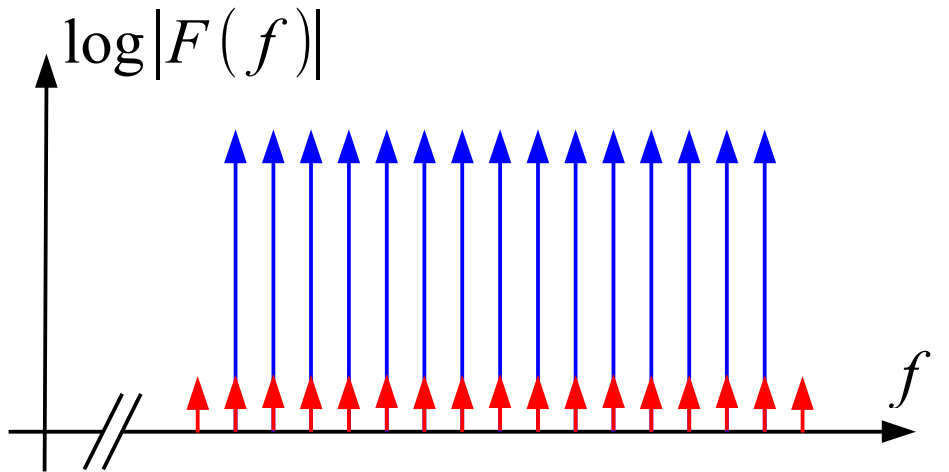
$$D \approx +5 \text{ ps}/(\text{nm}\cdot\text{km}) \quad \Delta f = 100 \text{ GHz}$$

$$\Delta\beta \approx -2.52 \text{ rd/km} \gg 2\alpha$$

$$l_{\text{eff}} \approx \frac{1}{|\Delta\beta|} \approx 0.4 \text{ km}$$

$$P_{\text{IP3}} \approx 2 \text{ W} = +33 \text{ dBm}$$

$$P_{\text{FWM}} = \frac{P^3}{P_{\text{IP3}}^2}$$



40 channels WDM × 100 Gb/s = 4 Tb/s