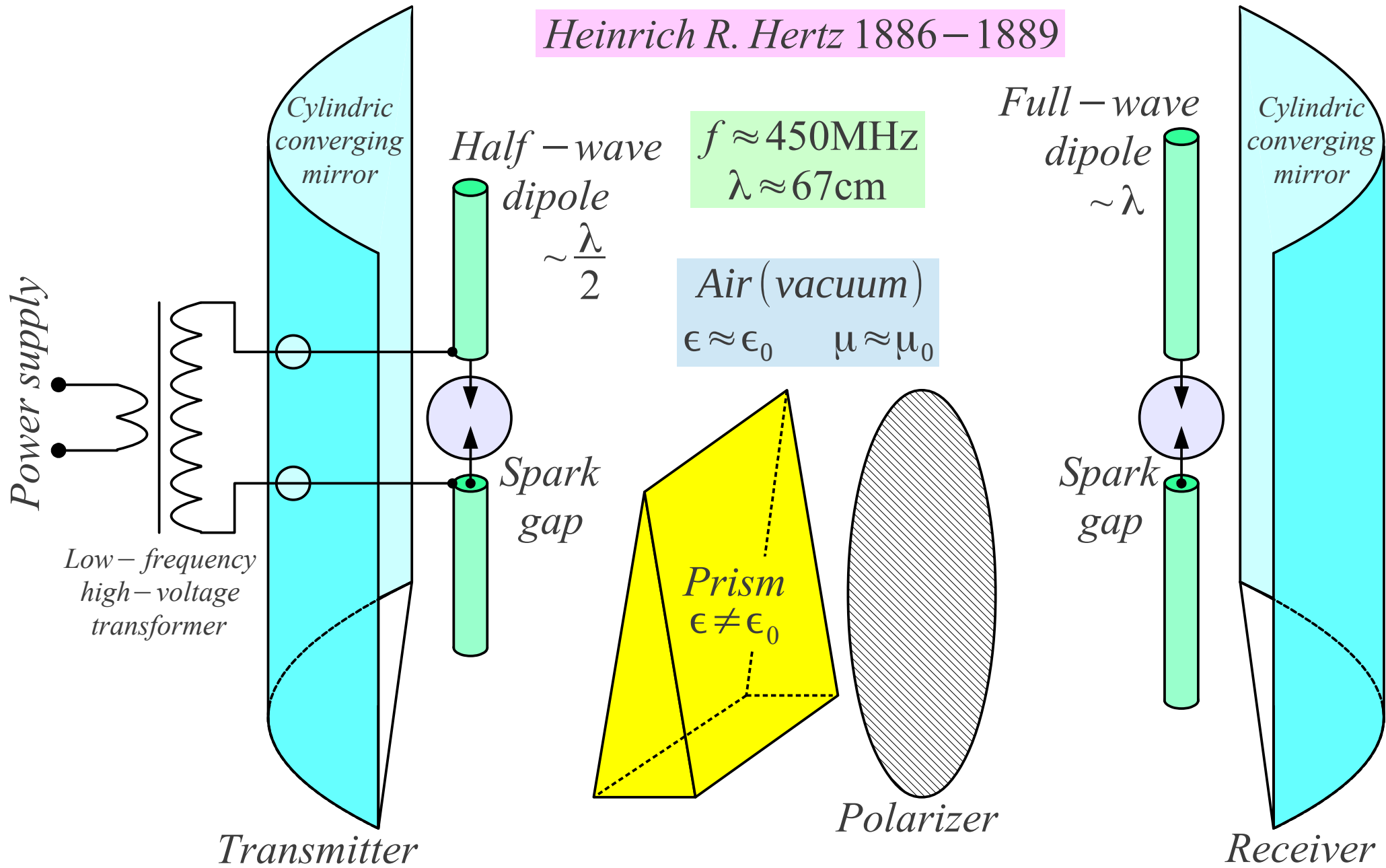


Communication Electronics

Lecture 10:

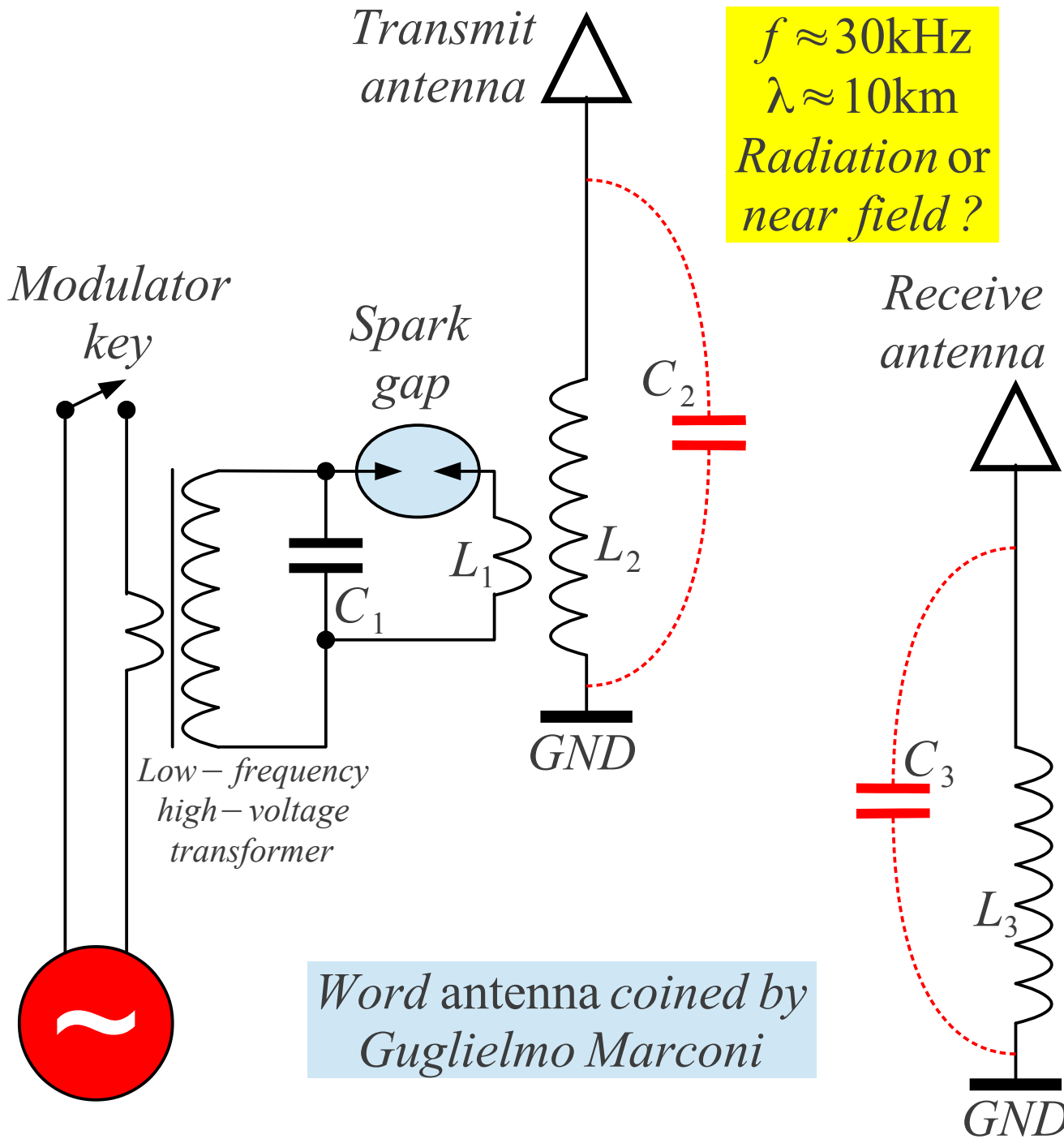
Transmitters and receivers

Heinrich R. Hertz 1886 – 1889



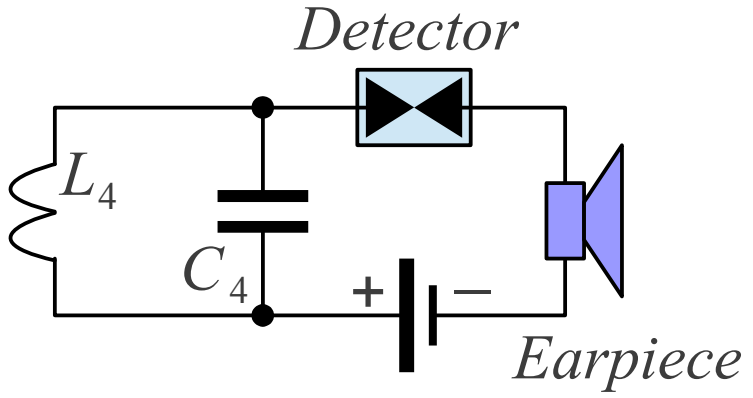
Radiation: $r \gg \frac{\lambda}{2\pi} \approx 10.6\text{cm}$

Hertz experiments



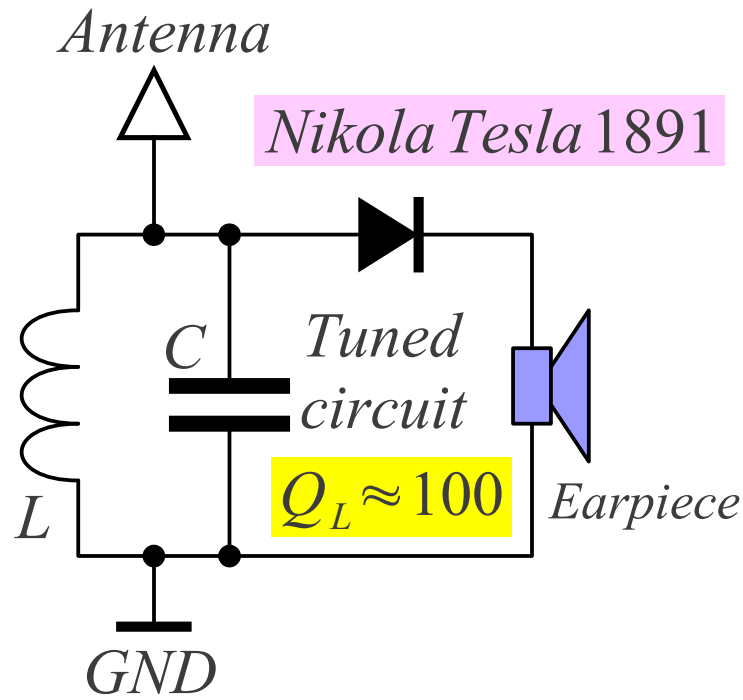
History of detectors	
Heinrich Hertz 1886	spark gap ~100V
Eduard Branley 1890	coherer ~10V
Jagdish Chandra Bose 1894	PbS crystal ~0.1V
Guglielmo Marconi 1902	magnetic det. ~1V
John Ambrose Fleming 1904	thermoionic diode ~0.3V
Armstrong + Meissner 1912	regenerative RX ~1mV
Edwin Armstrong 1922	super-regen. RX ~1μV

Word antenna coined by
Guglielmo Marconi



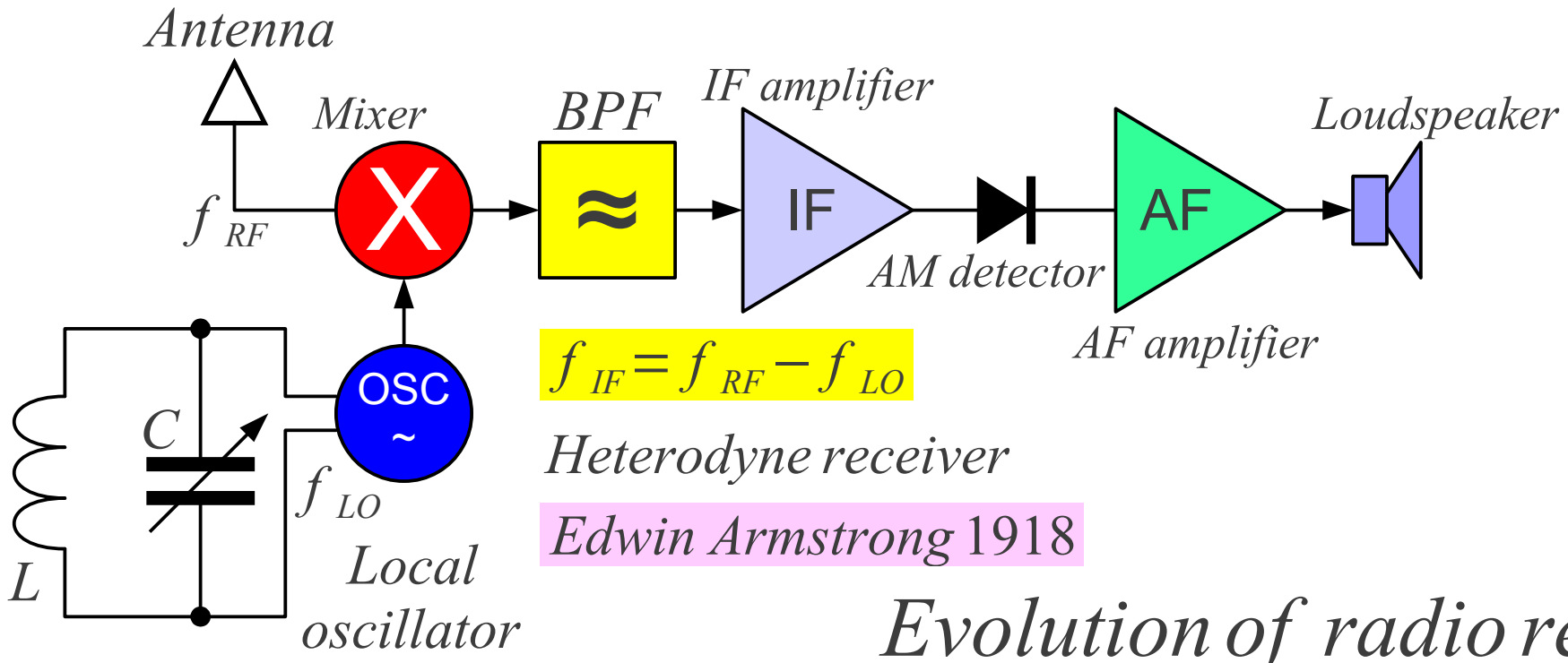
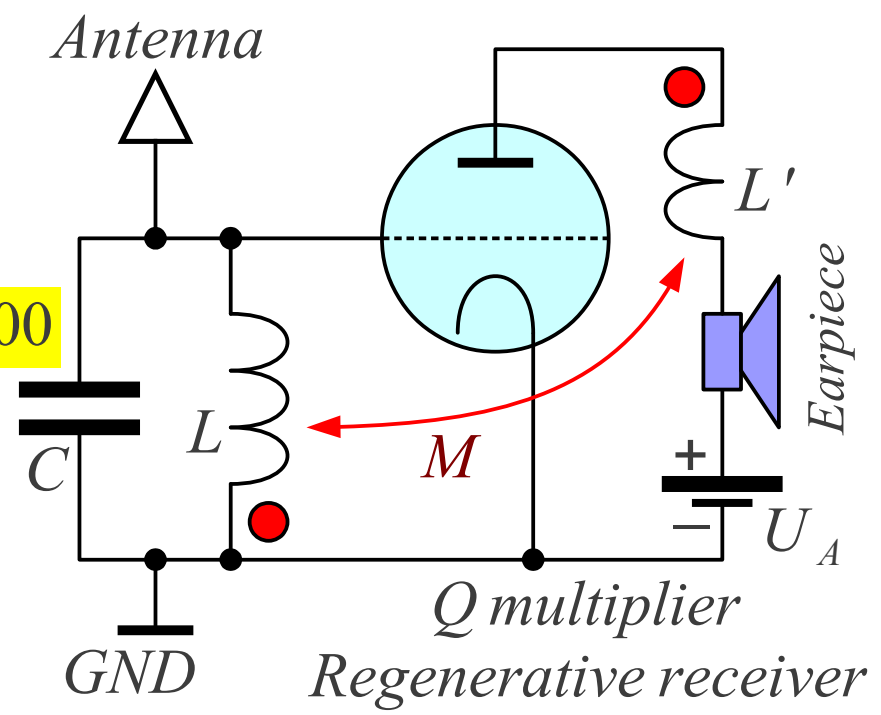
Four tuned circuits (Nikola Tesla)

Meissner / Armstrong 1912

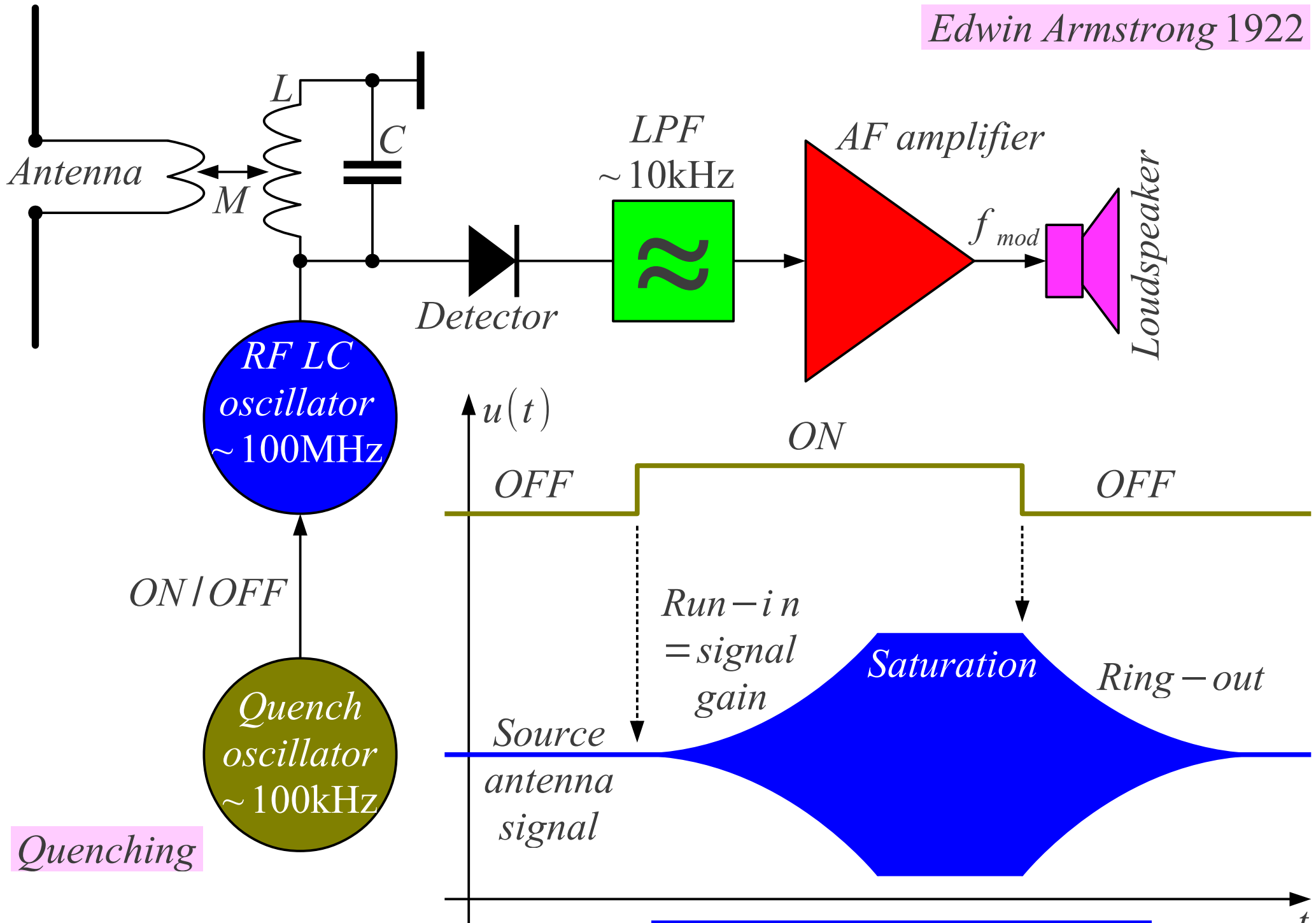


$$B = \frac{f_0}{Q_L}$$

$$Q_L \approx 1000$$



Evolution of radio receivers



Quenching

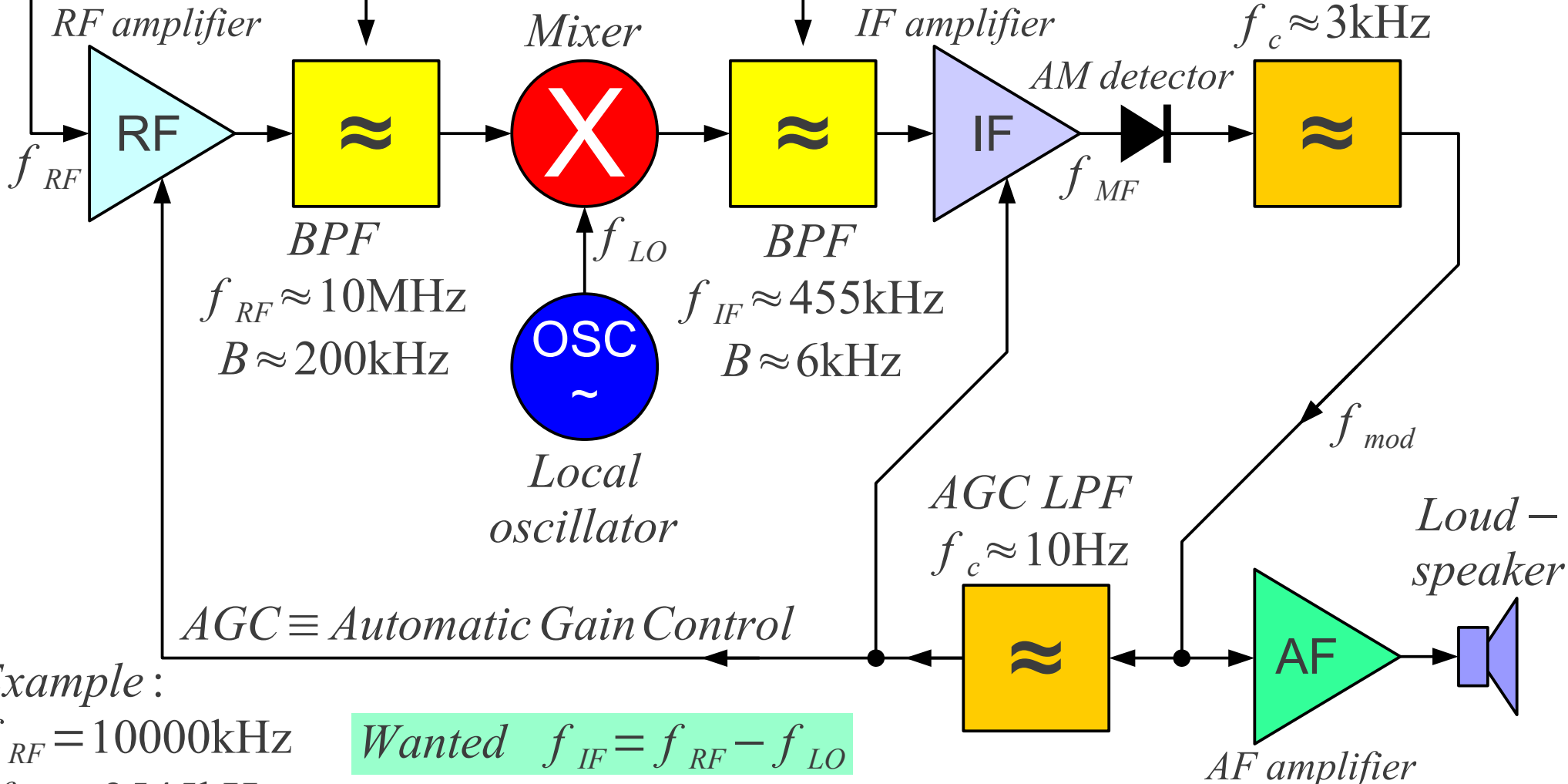
Super-regenerative RX

Stable gain $G > 100\text{dB} + \text{AGC}!$

Antenna

Image reject

Modulation bandwidth



Example :

$f_{RF} = 10000\text{kHz}$
 $f_{LO} = 9545\text{kHz}$
 $f_I = 9090\text{kHz}$

Wanted $f_{IF} = f_{RF} - f_{LO}$

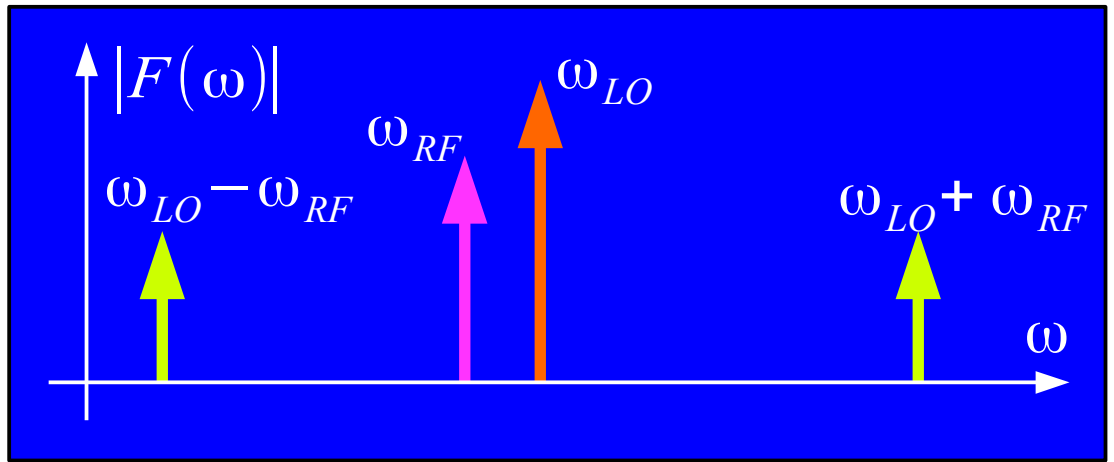
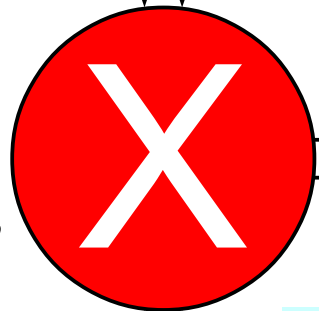
Image $f_{IF} = f_{LO} - f_I$

Heterodyne AM receiver

$$u_{RF} = A_{RF} \cdot \cos \omega_{RF} t$$

$$u_{LO} = A_{LO} \cdot \cos \omega_{LO} t$$

Analog multiplier as frequency mixer



$K_m [V^{-1}] \equiv$ multiplier factor

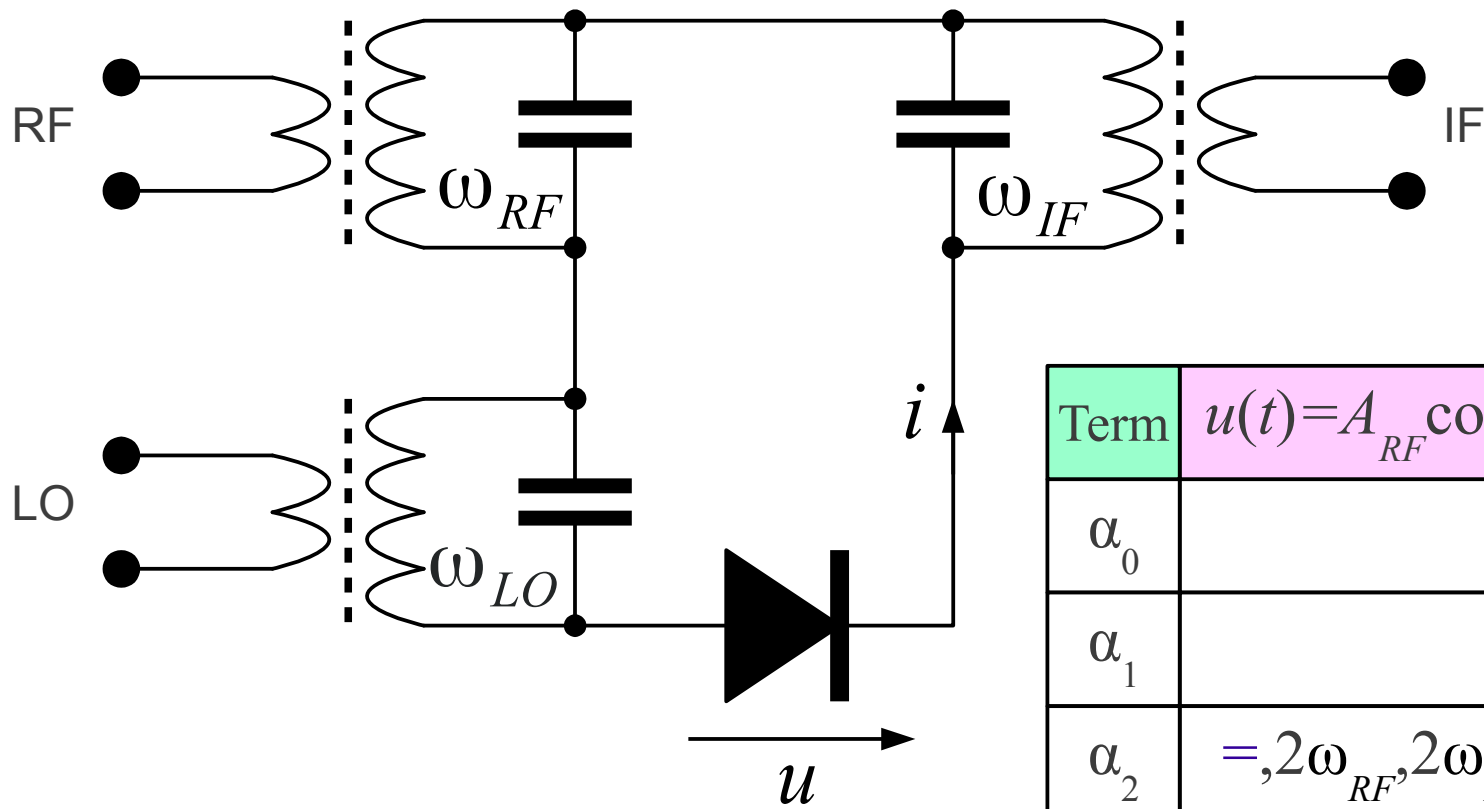
$$u_{IF} = K_m \cdot u_{RF} \cdot u_{LO}$$

$$u_{IF} = K_m A_{RF} A_{LO} \cos \omega_{RF} t \cos \omega_{LO} t$$

$$\cos x \cos y = \frac{1}{2} \cdot [\cos(y+x) + \cos(y-x)]$$

$$u_{IF} = \frac{K_m A_{RF} A_{LO}}{2} \cdot [\cos(\omega_{LO} + \omega_{RF}) t + \cos(\omega_{LO} - \omega_{RF}) t]$$

Multiplier as frequency mixer (modulator)

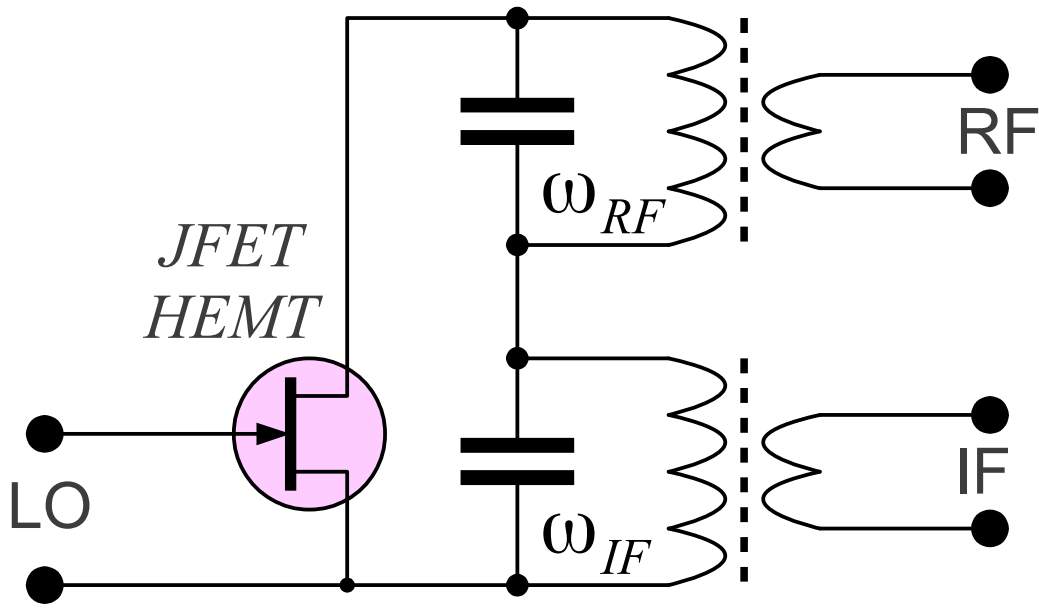
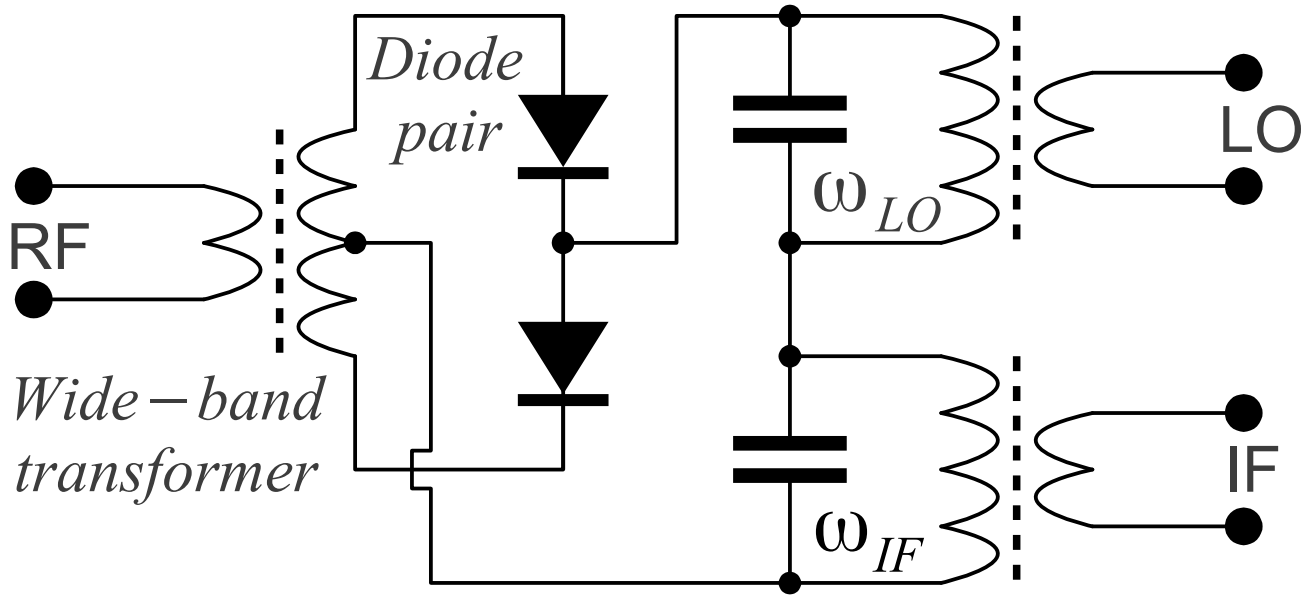


$$\begin{aligned}
 i &= I_S \left(e^{\frac{u|Q_e|}{nk_B T}} - 1 \right) = \\
 &= \alpha_0 + \alpha_1 \cdot u + \alpha_2 \cdot u^2 + \\
 &+ \alpha_3 \cdot u^3 + \alpha_4 \cdot u^4 + \alpha_5 \cdot u^5 + \\
 &+ \alpha_6 \cdot u^6 + \alpha_7 \cdot u^7 + \dots
 \end{aligned}$$

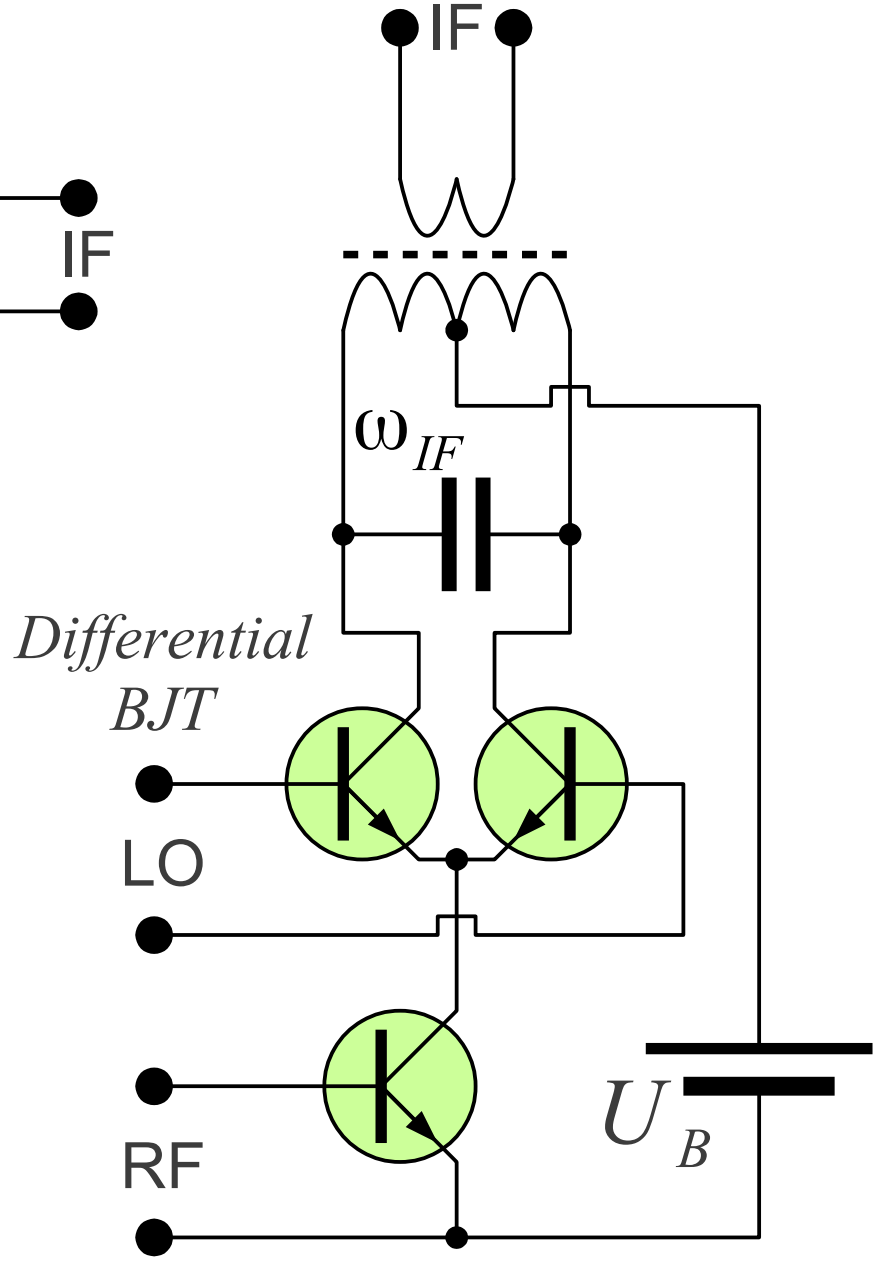
Term	$u(t) = A_{RF} \cos(\omega_{RF} t) + A_{LO} \cos(\omega_{LO} t)$
α_0	=
α_1	ω_{RF}, ω_{LO}
α_2	$=, 2\omega_{RF}, 2\omega_{LO}, \omega_{RF} + \omega_{LO}, \omega_{LO} - \omega_{RF}$
α_3	$\omega_{RF}, \omega_{LO}, 3\omega_{RF}, 3\omega_{LO}, 2\omega_{RF} + \omega_{LO},$ $2\omega_{RF} - \omega_{LO}, \omega_{RF} + 2\omega_{LO}, 2\omega_{LO} - \omega_{RF}$
α_4	$=, 2\omega_{RF}, 2\omega_{LO}, \omega_{RF} + \omega_{LO}, \omega_{LO} - \omega_{RF},$ $4\omega_{RF}, 4\omega_{LO}, 3\omega_{RF} + \omega_{LO},$ $2\omega_{RF} + 2\omega_{LO}, \omega_{RF} + 3\omega_{LO}, 3\omega_{RF} - \omega_{LO},$ $2\omega_{LO} - 2\omega_{RF}, 3\omega_{LO} - \omega_{RF}$
α_5	$\dots 5\omega_{RF}, 5\omega_{LO} \dots$

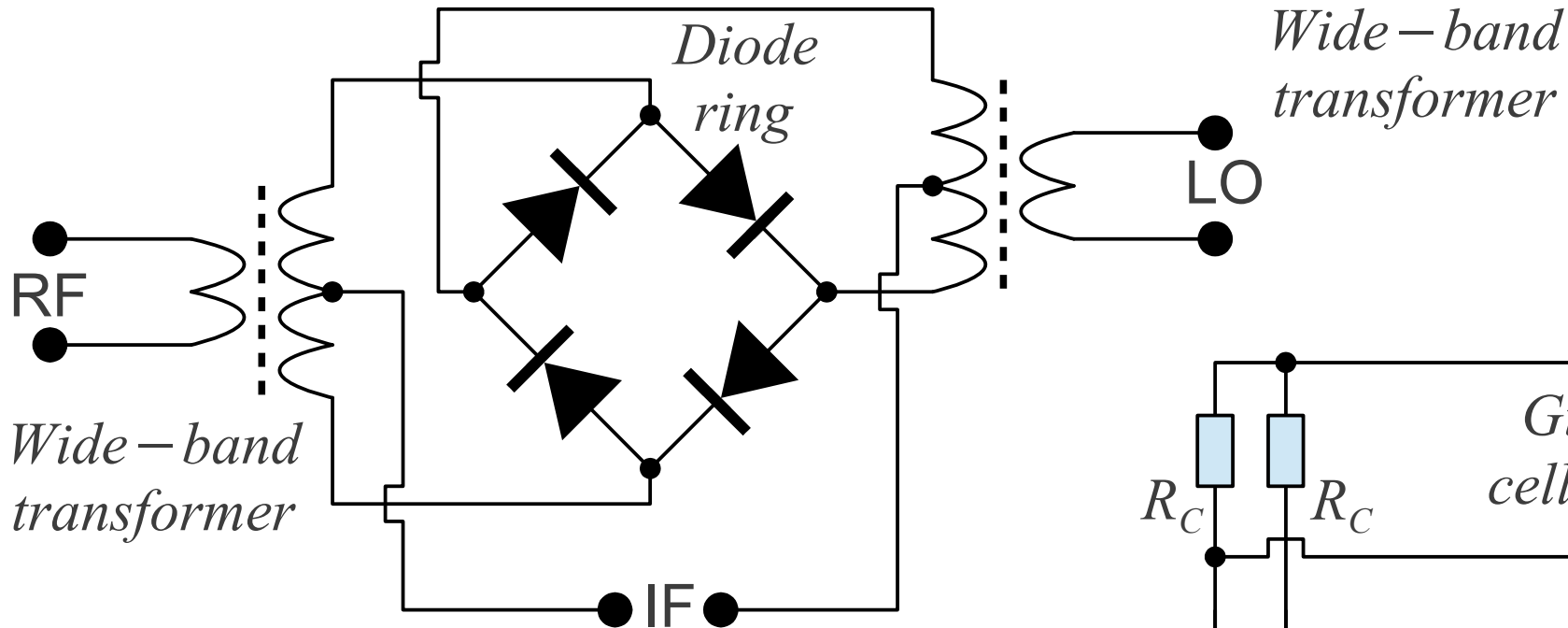
Single – diode mixer

Balanced mixer

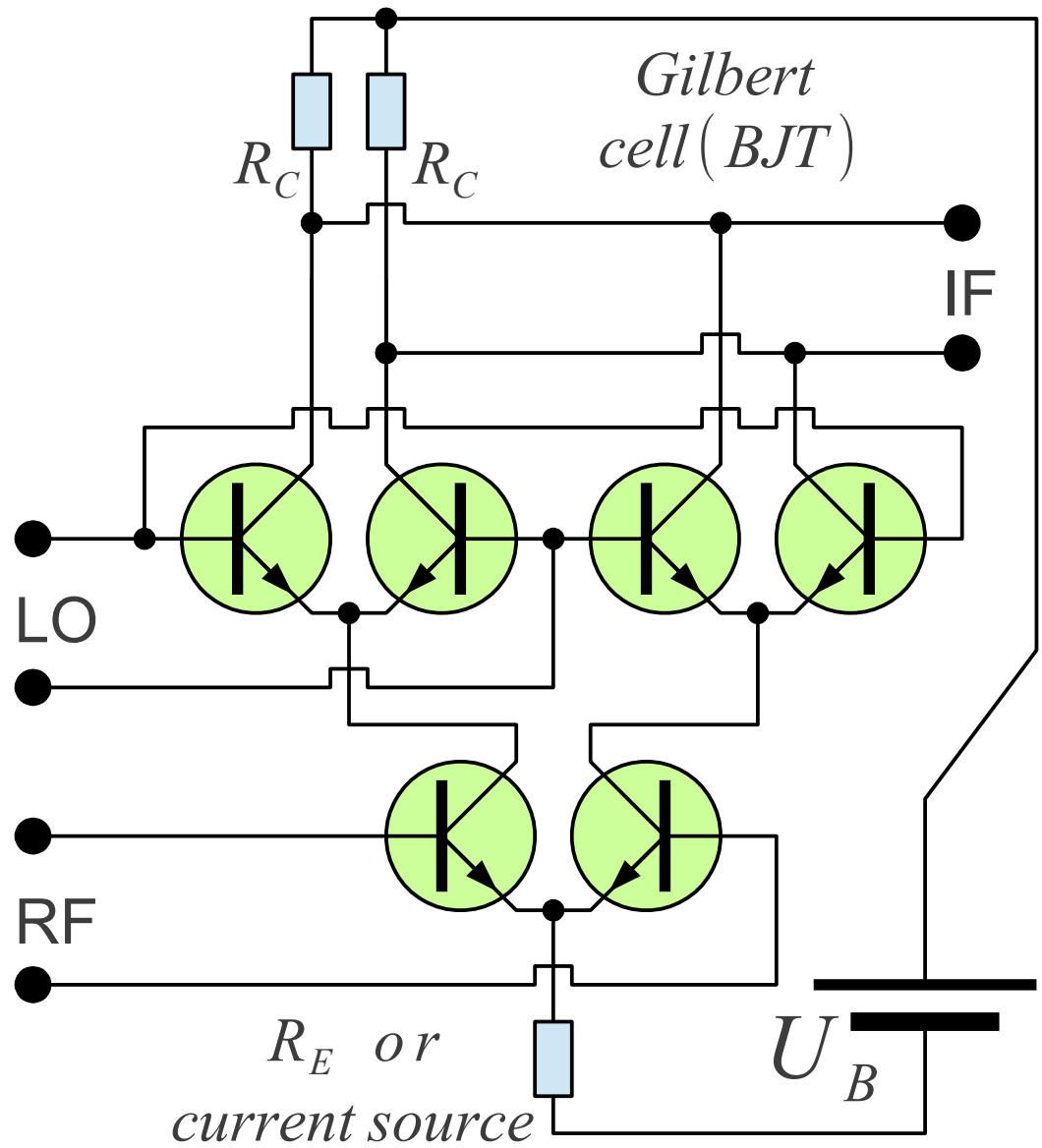
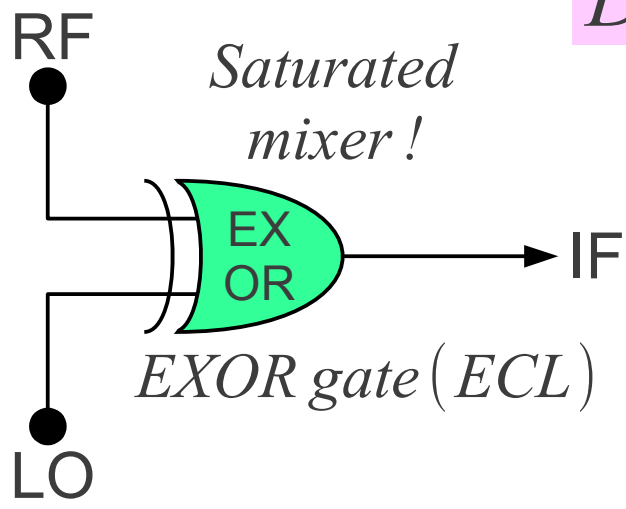


Single – balanced mixers





DBM



Double – balanced mixers

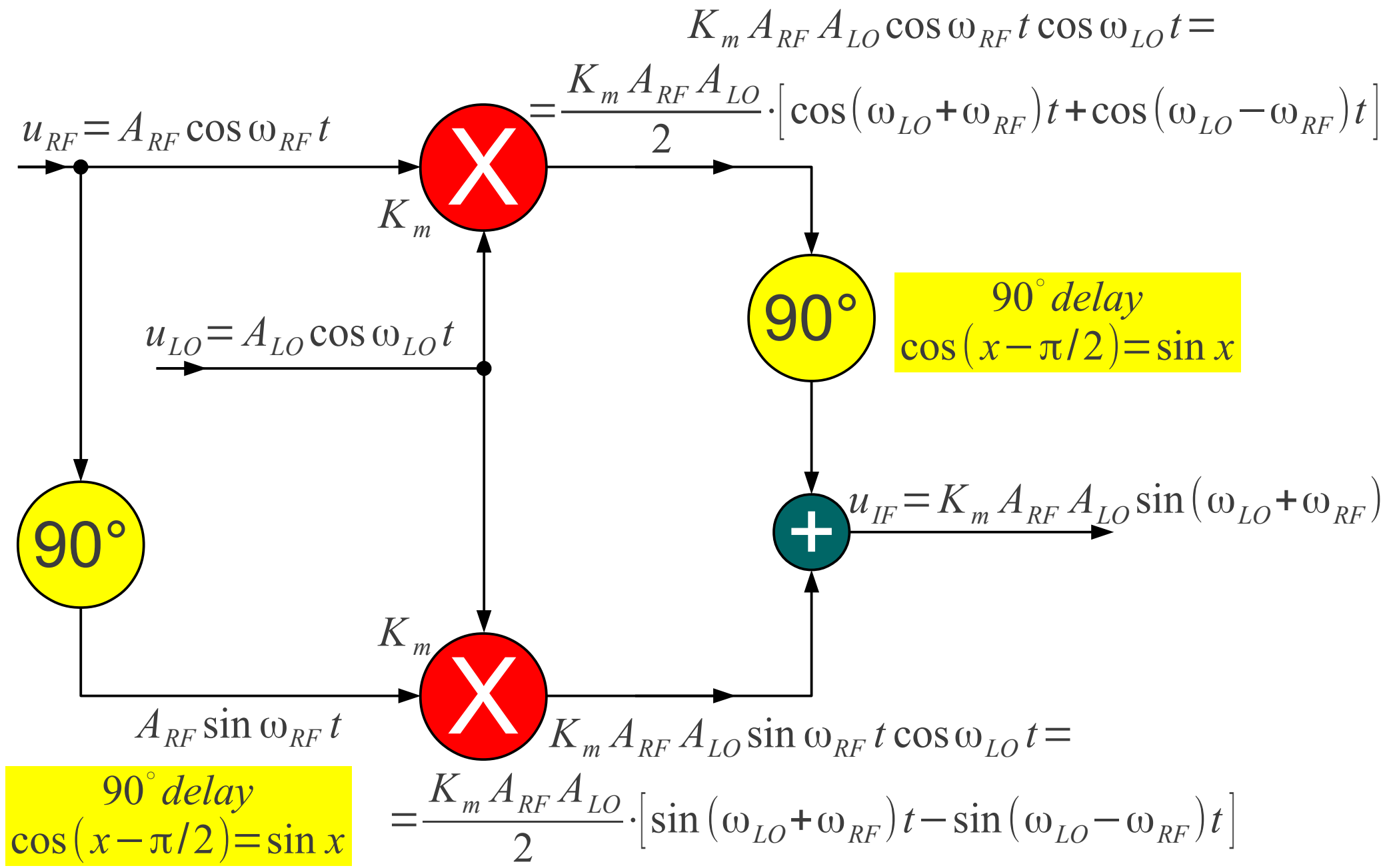


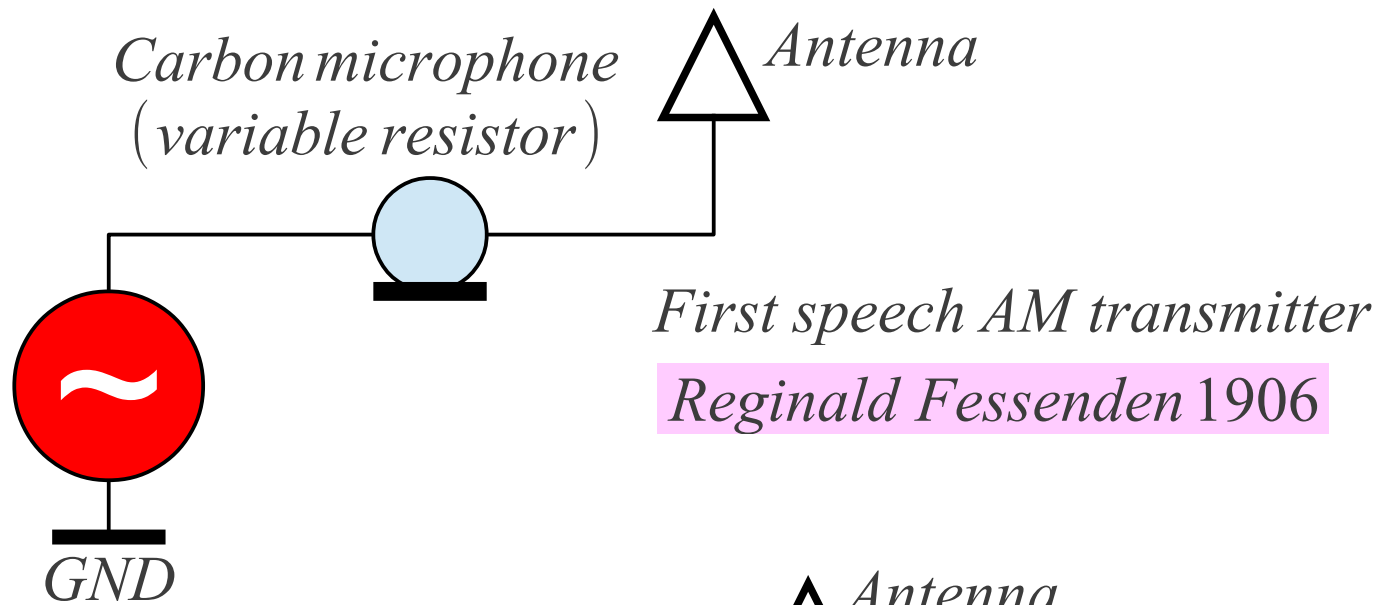
Image – reject mixer

Ernst Alexanderson 1904

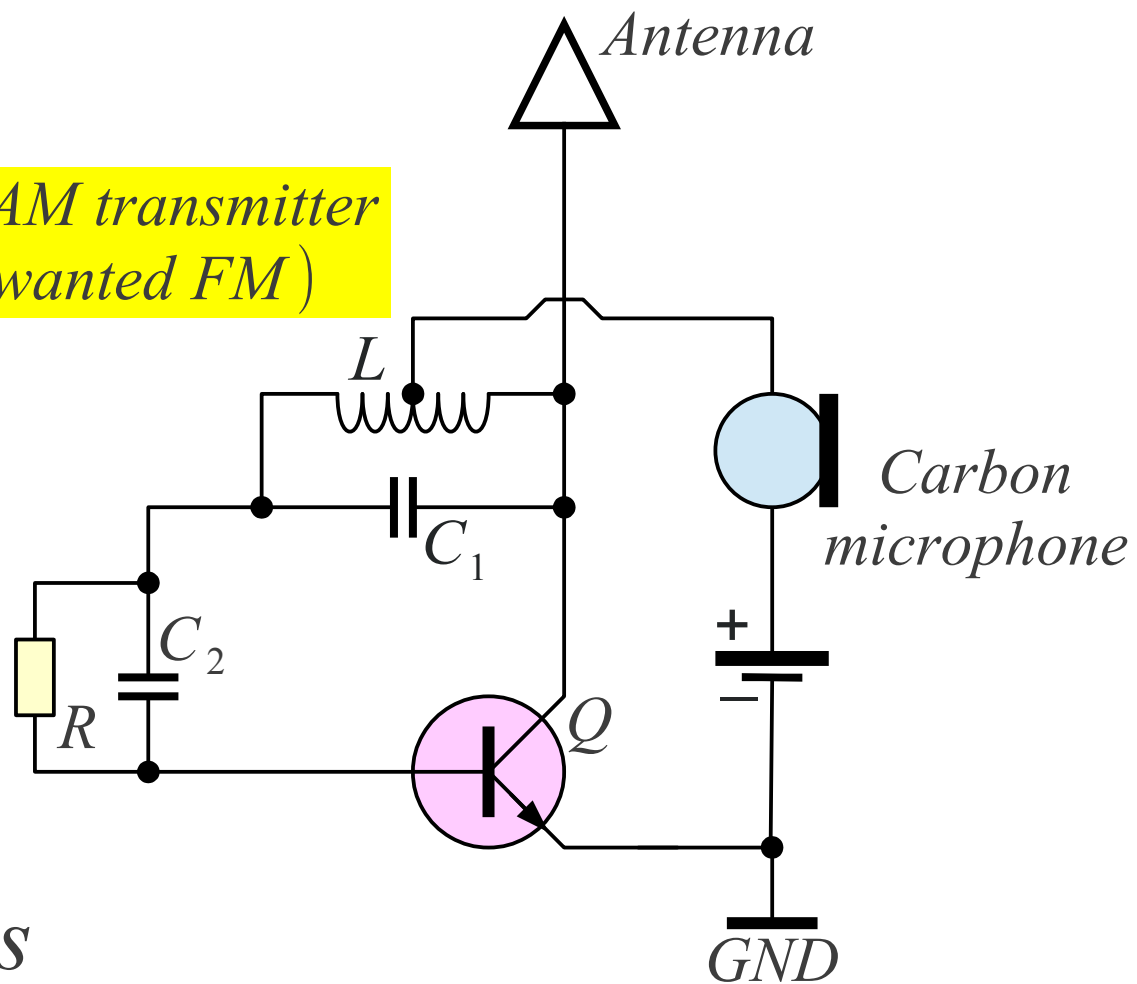
Electro-mechanical generator $f \approx 50\text{kHz}$

Nikola Tesla 1891
 $f \approx 15\text{kHz}$

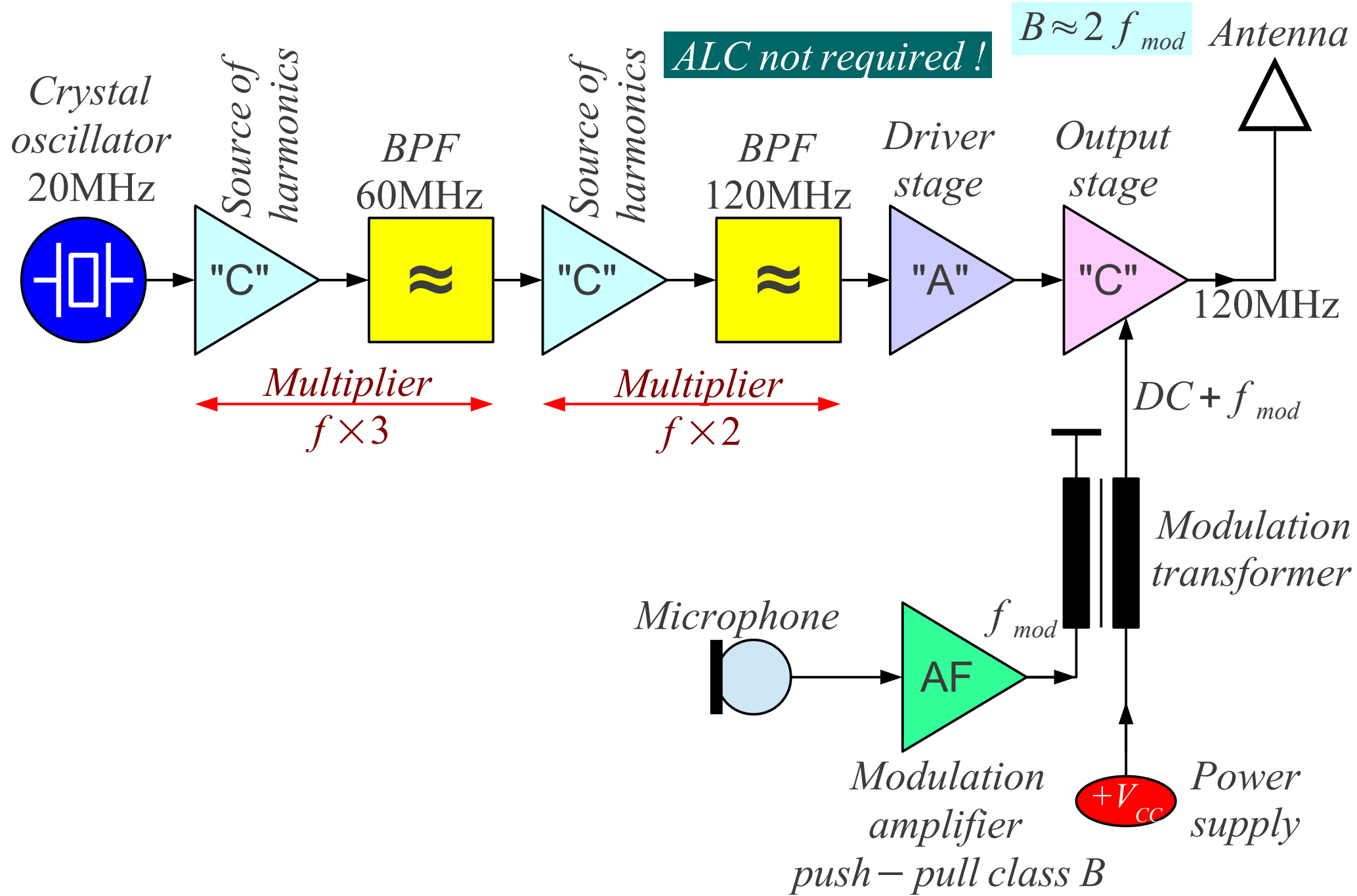
Electro-mechanical RF generator design survives today as stepper motors!



Simple AM transmitter (+ unwanted FM)

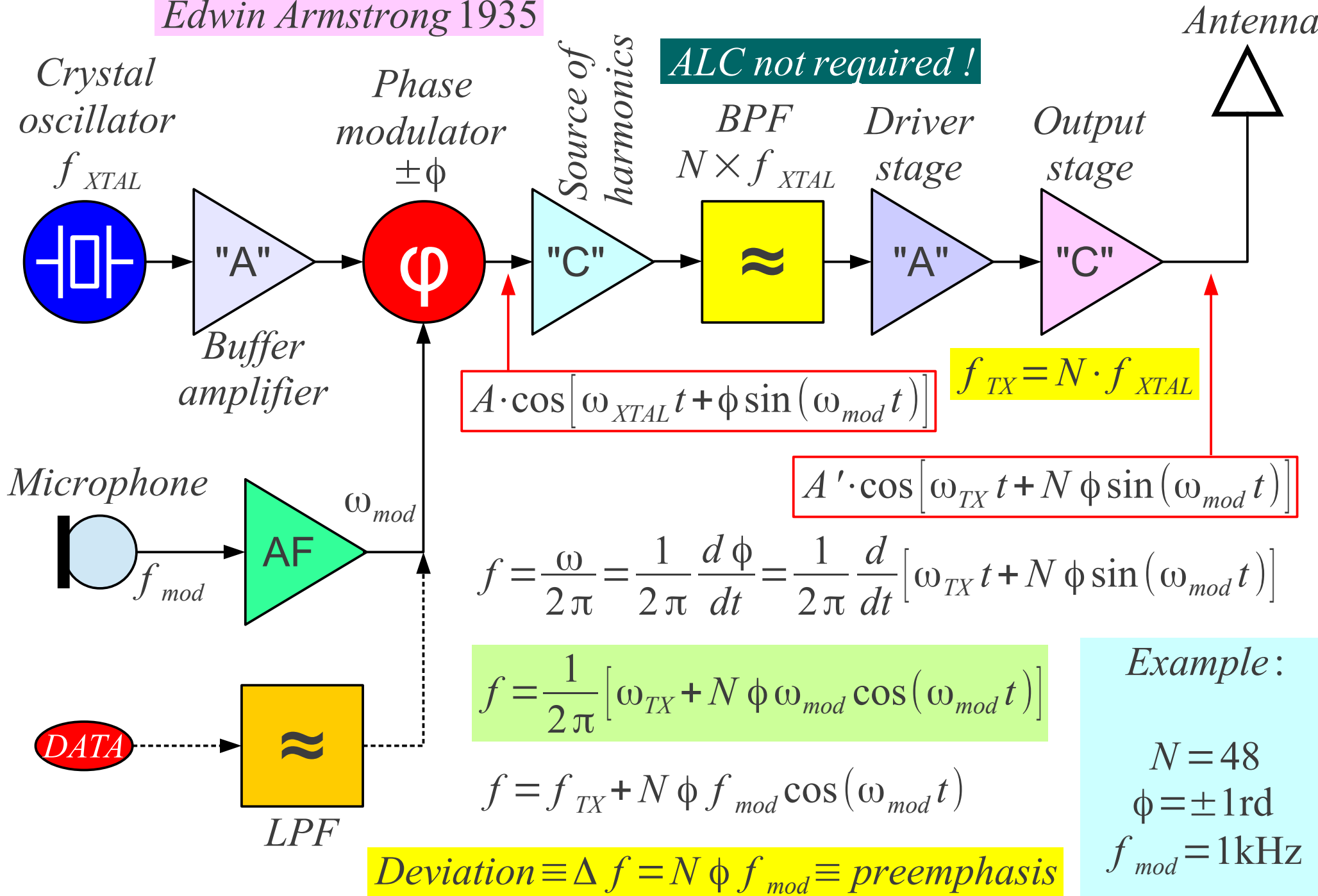


AM (speech) transmitters



AM transmitter with output modulation

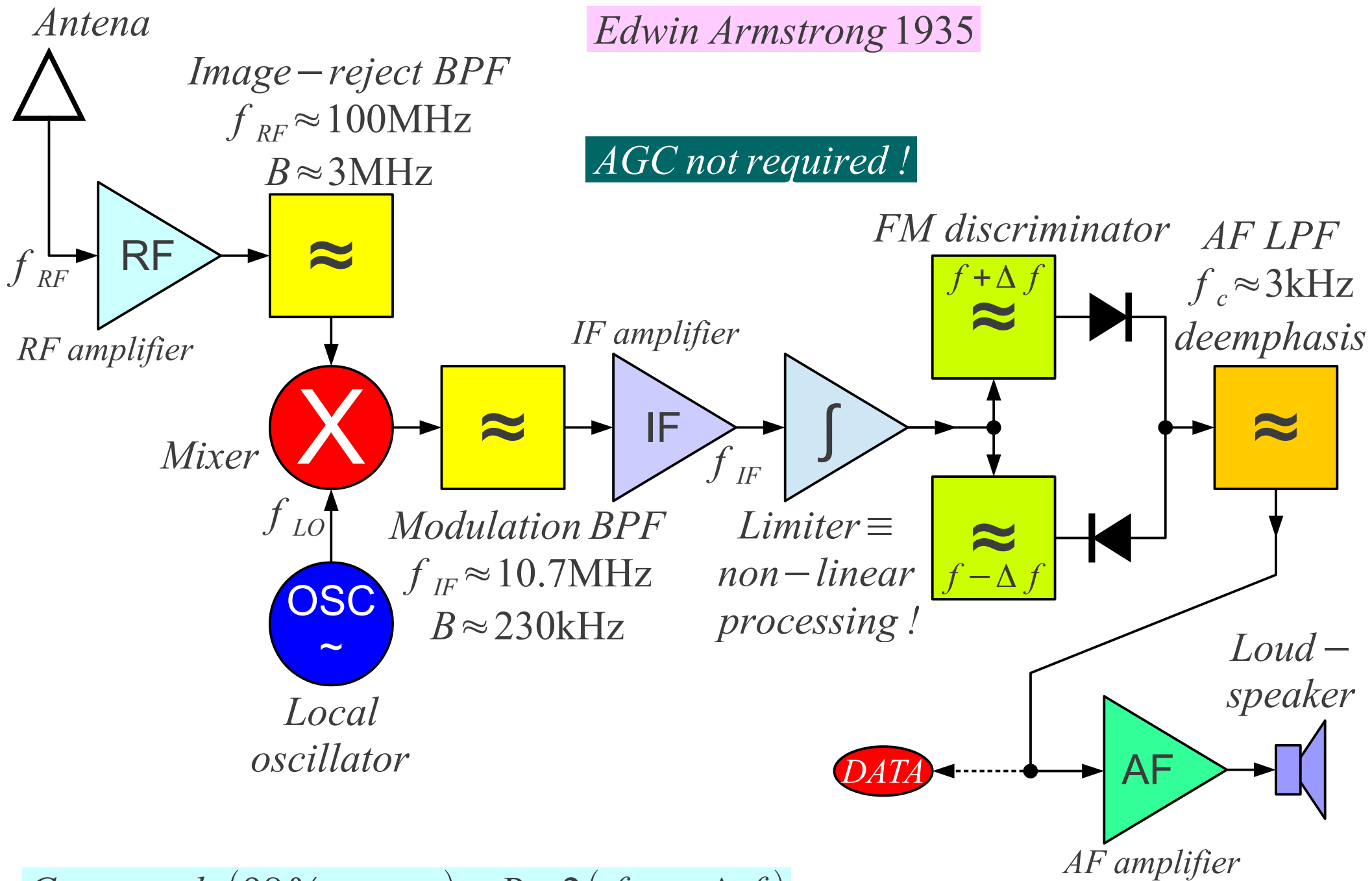
Edwin Armstrong 1935



Frequency (phase) – modulated transmitter $\Delta f = \pm 48kHz$

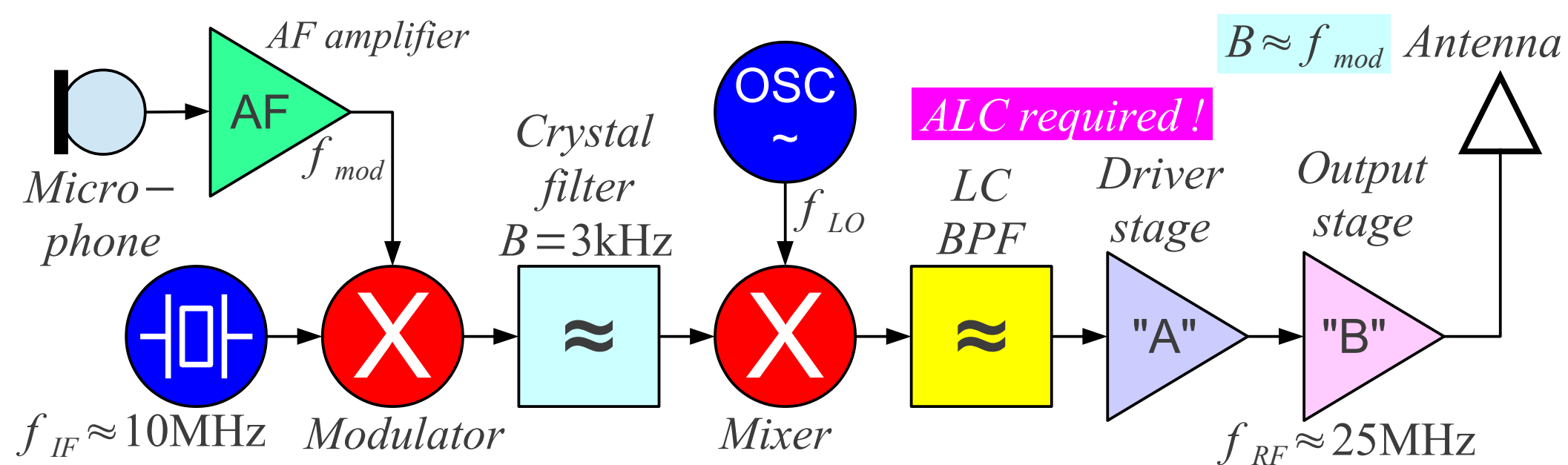
Edwin Armstrong 1935

AGC not required!

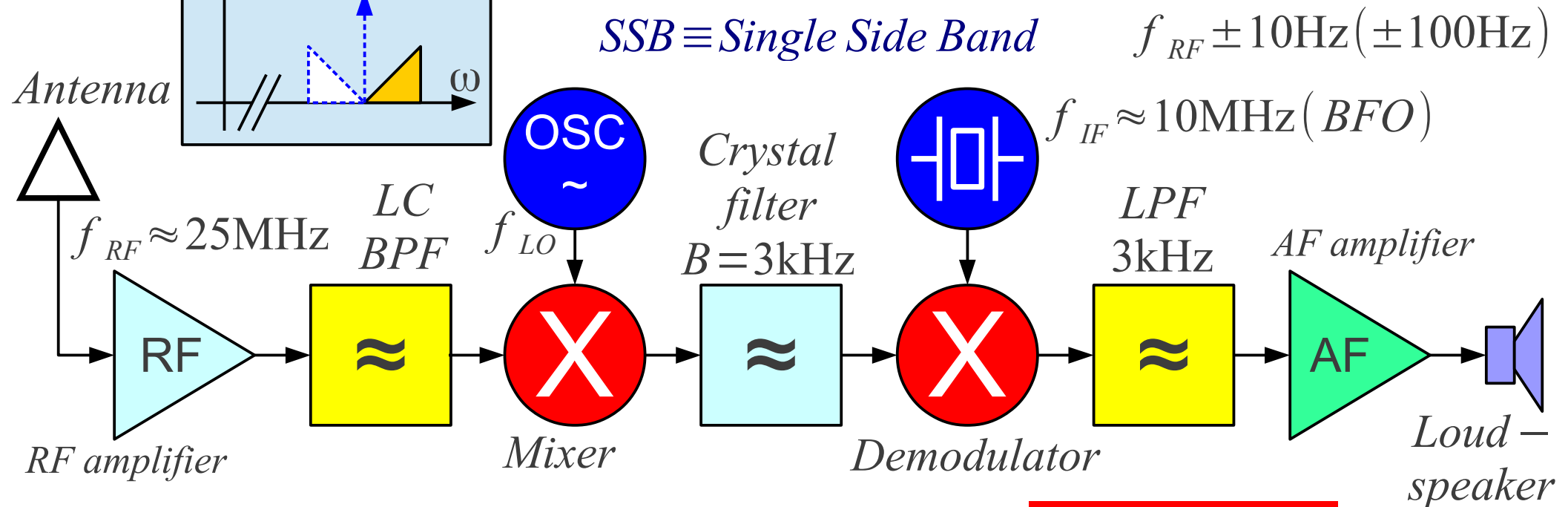


Carson rule (98% power): $B \approx 2(f_{mod} + \Delta f)$

Heterodyne FM receiver



Frequency accuracy of all oscillators?



Single-sideband AM

$\log(S/N)_{AF}$

FM index: $m = \frac{\Delta f}{f_{mod}}$

$\left(\frac{S}{N}\right)_{AF} \approx 3 m^2 \cdot \left(\frac{S}{N}\right)_{RF}$

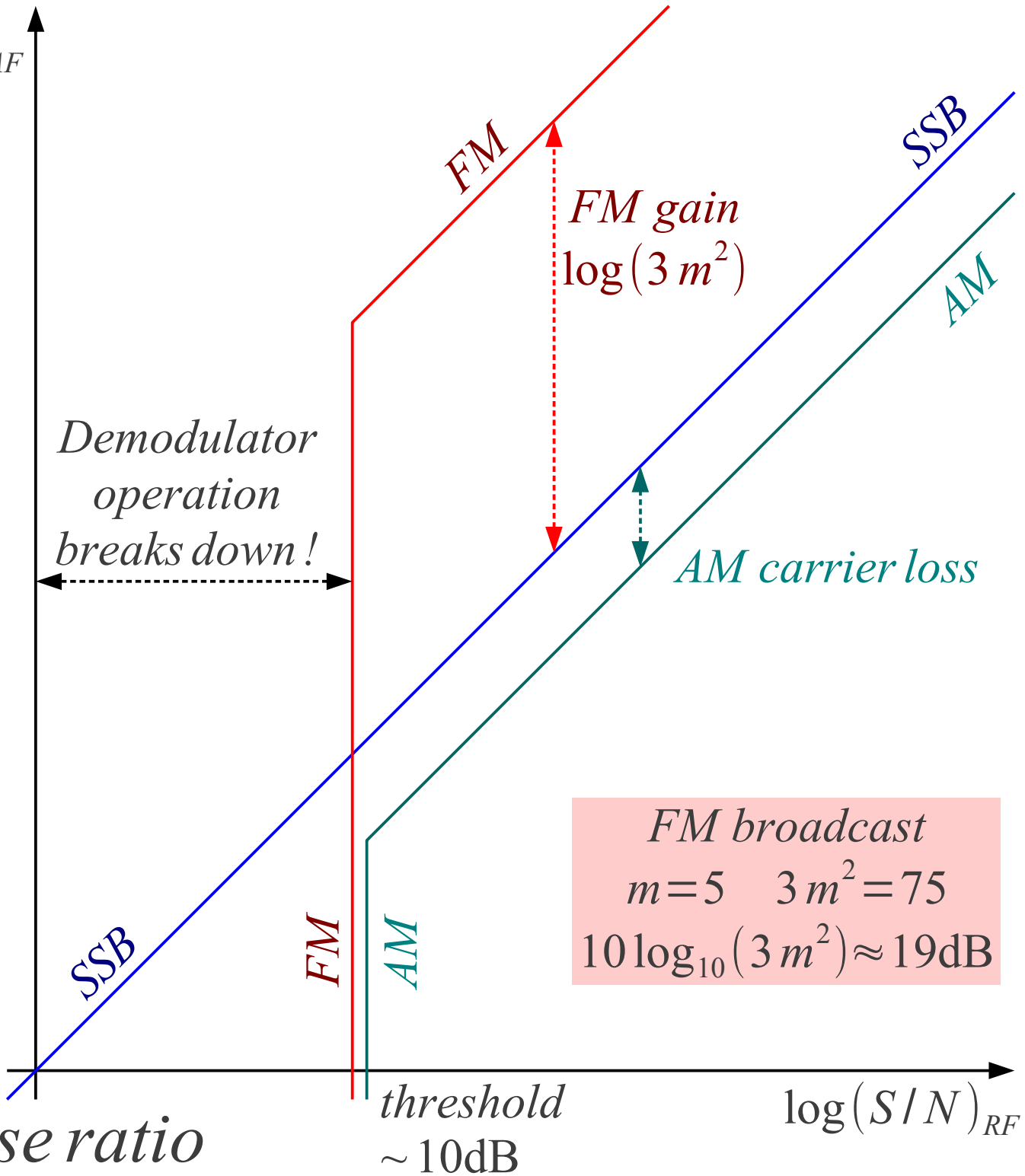
Usually: $m = 2 \dots 5$

$B \approx 2(1+m) \cdot f_{mod}$

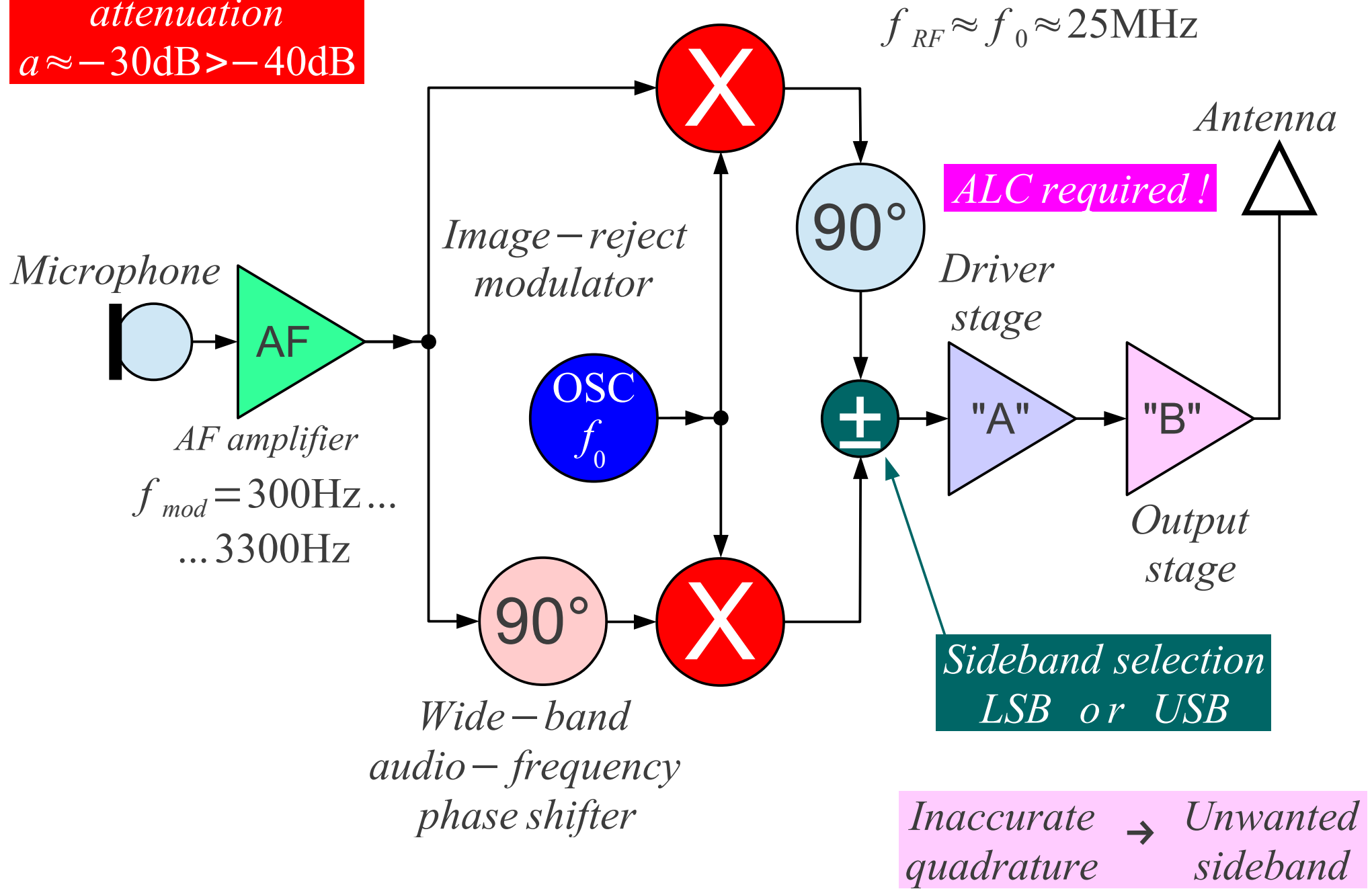
SSB processing is fully linear!

AM index:

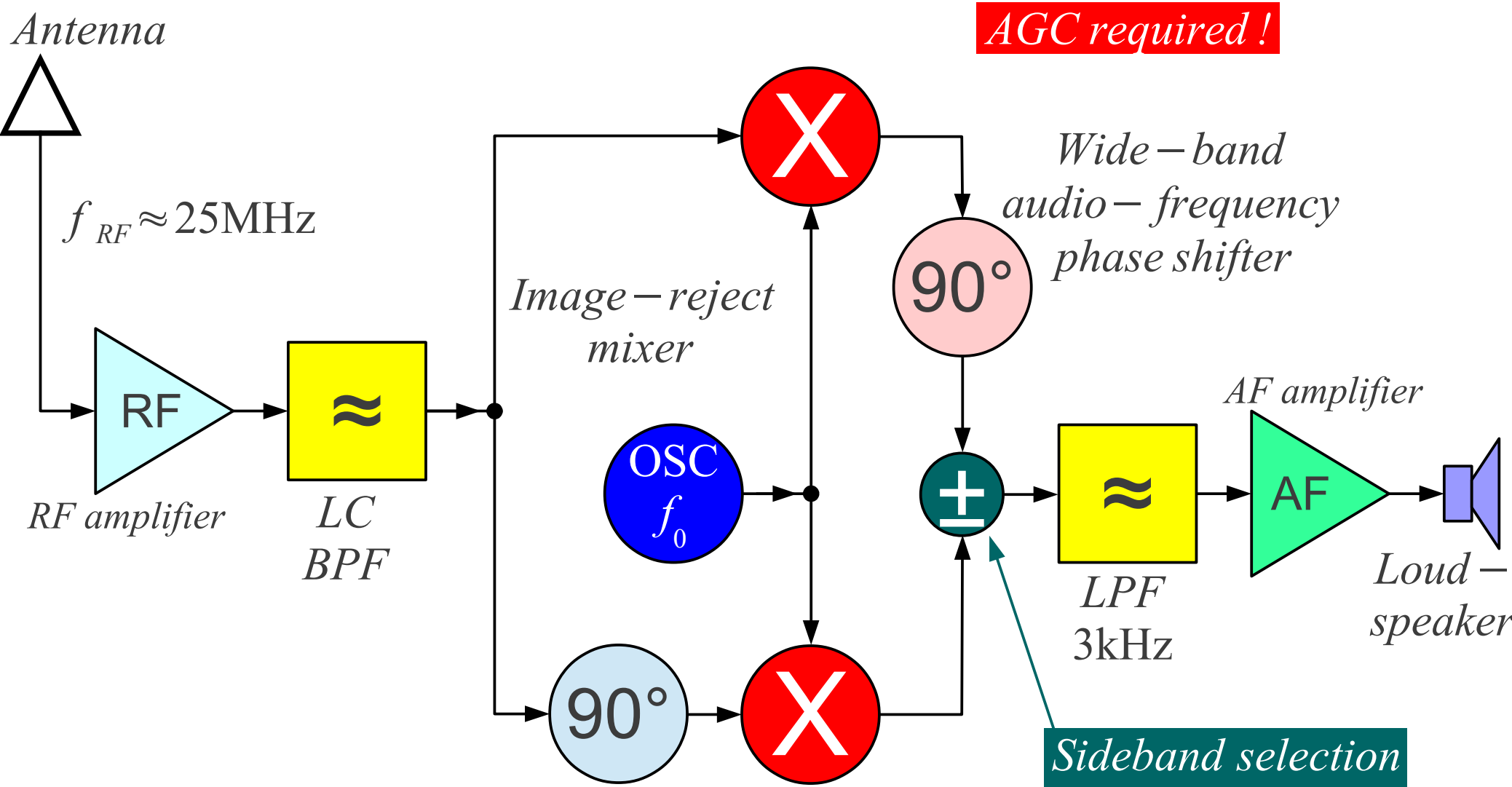
$0 < m \leq 100\%$



*Unwanted sideband
attenuation
 $a \approx -30\text{dB} > -40\text{dB}$*

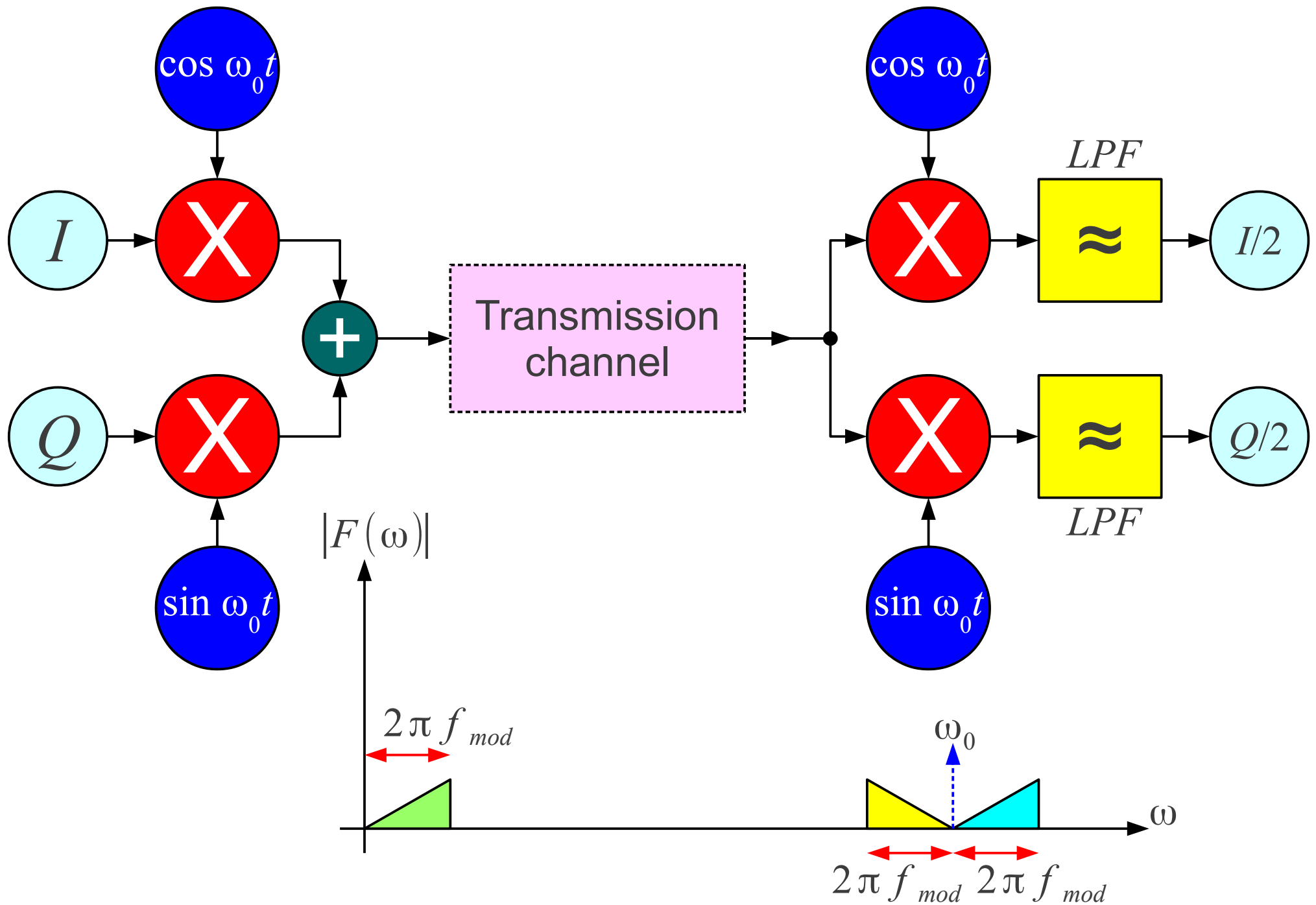


SSB transmitter with image rejection



Unwanted sideband attenuation
 $a \approx -30\text{dB} > -40\text{dB}$

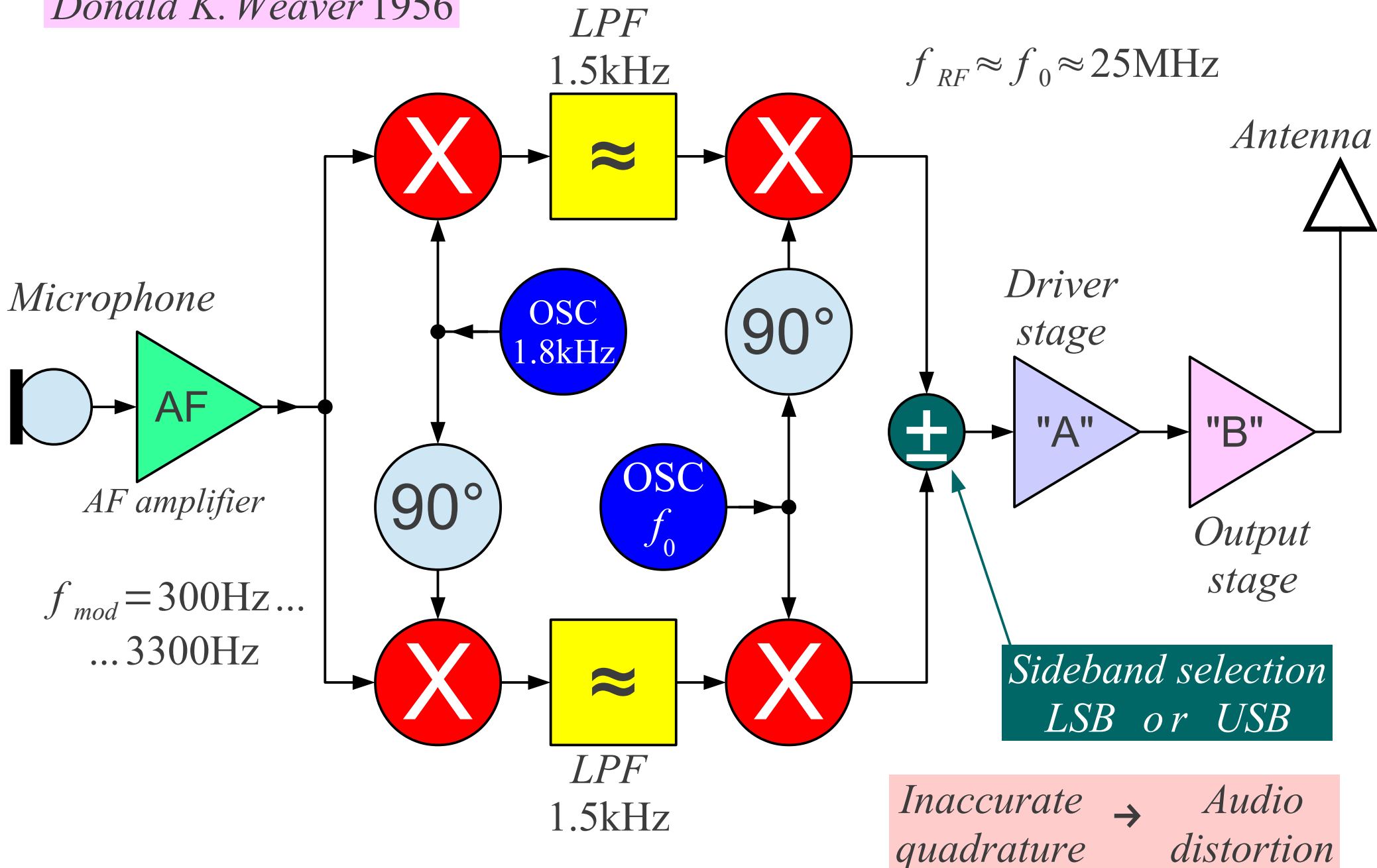
SSB receiver with image rejection



Quadrature amplitude modulation (QAM)

Donald K. Weaver 1956

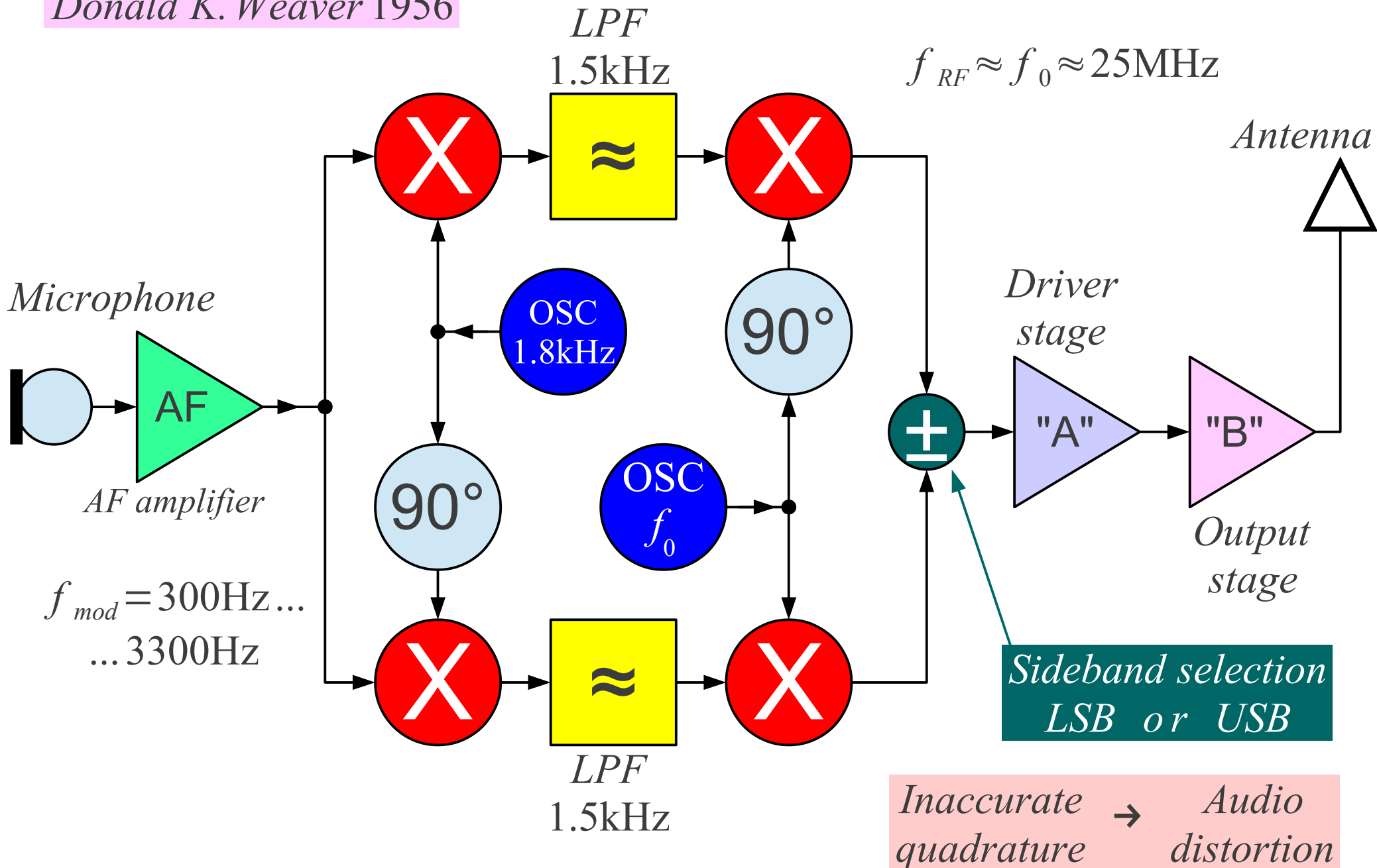
ALC required!



Weaver SSB transmitter

Donald K. Weaver 1956

ALC required!



Weaver SSB transmitter

Weaver 1956 → Zero-IF 1996

Inaccurate quadrature → Audio distortion

Antenna

$f_{RF} \approx f_0 \approx 25\text{MHz}$

RF amplifier

LC BPF

X

LPF 1.5kHz

X

$f_{mod} = 300\text{Hz} \dots \dots 3300\text{Hz}$

90°

OSC 1.8kHz

AF amplifier

RF amplifier

LC BPF

OSC f_0

90°

Loud-speaker

X

LPF 1.5kHz

X

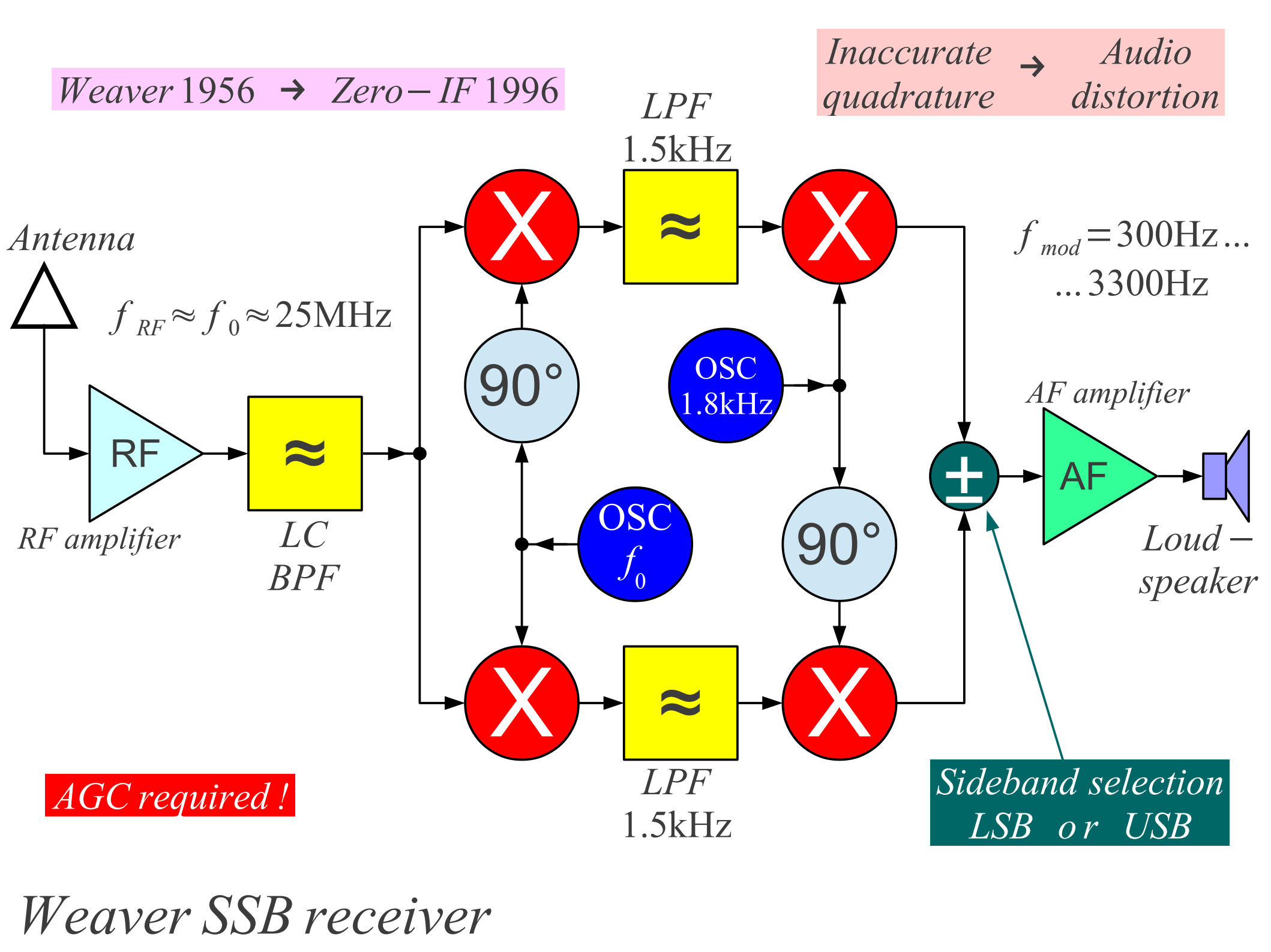
+

AF

AGC required!

Sideband selection LSB or USB

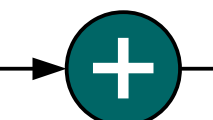
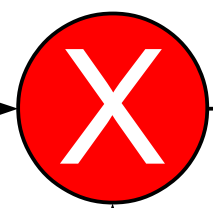
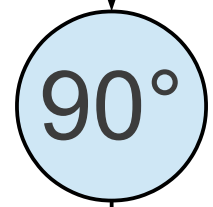
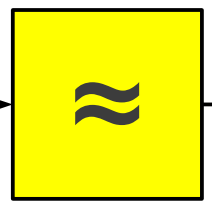
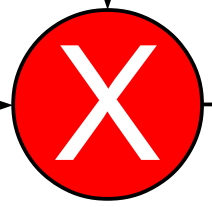
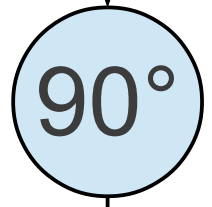
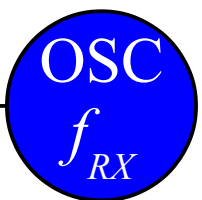
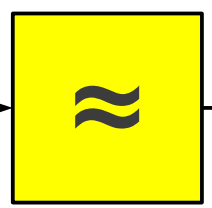
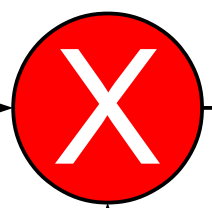
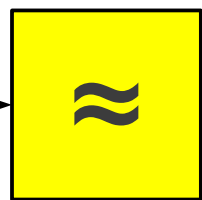
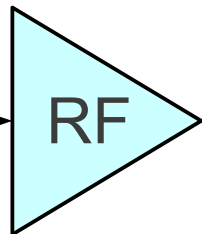
Weaver SSB receiver



Antenna

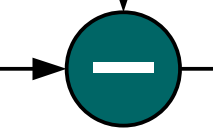
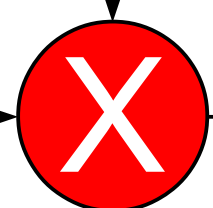
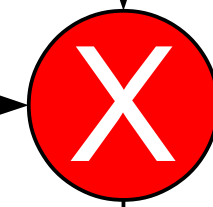
f_{TX}

AGC required!



I

Q'

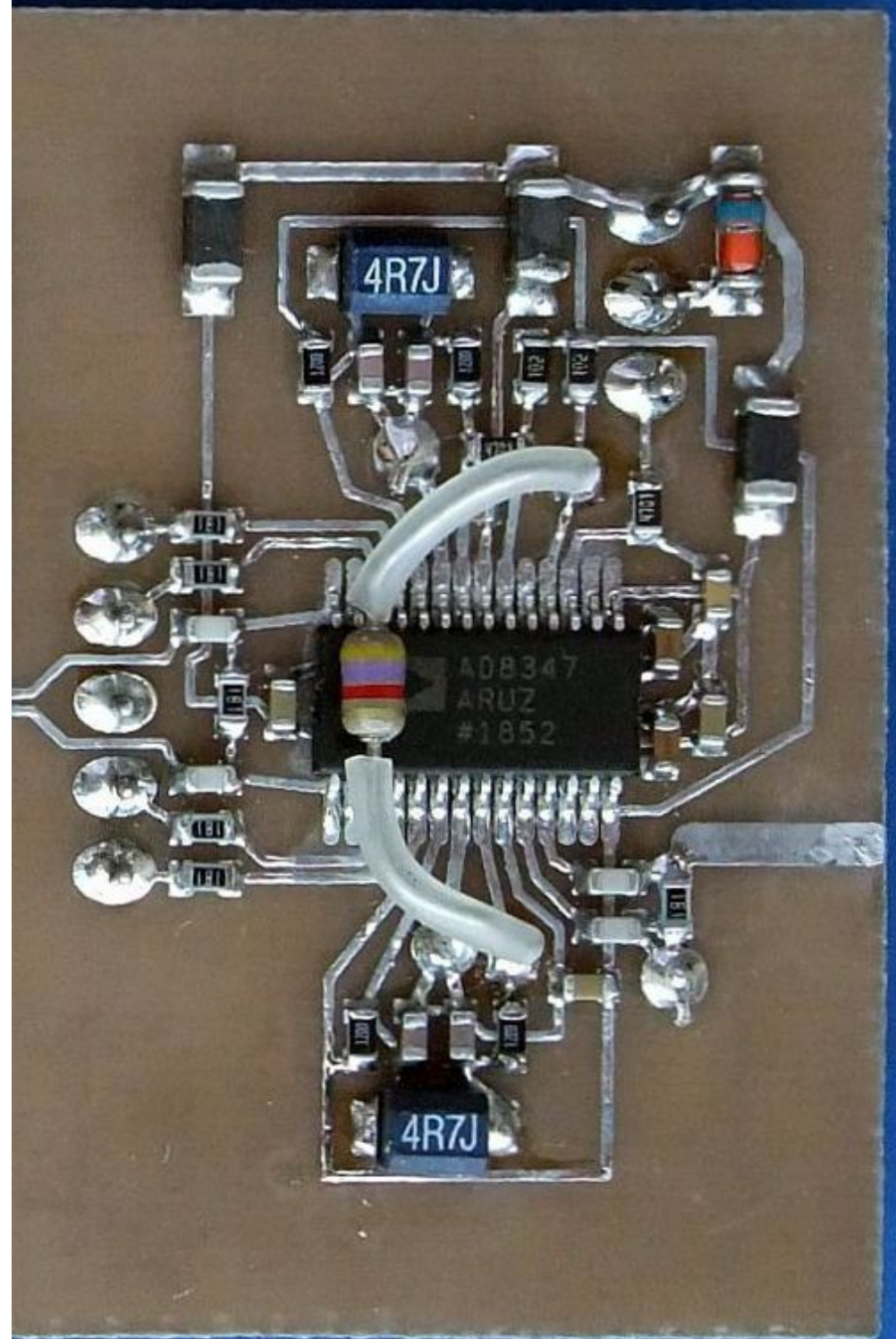
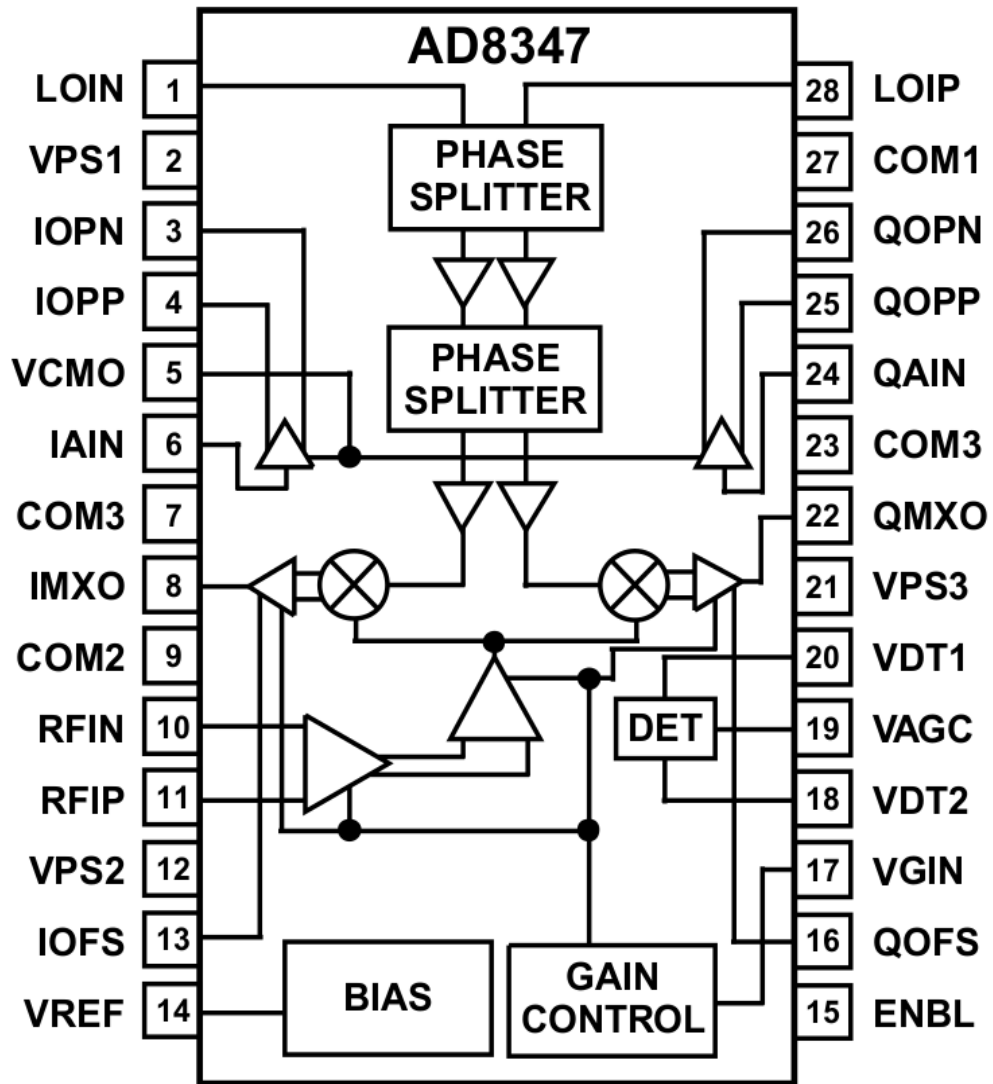


Q

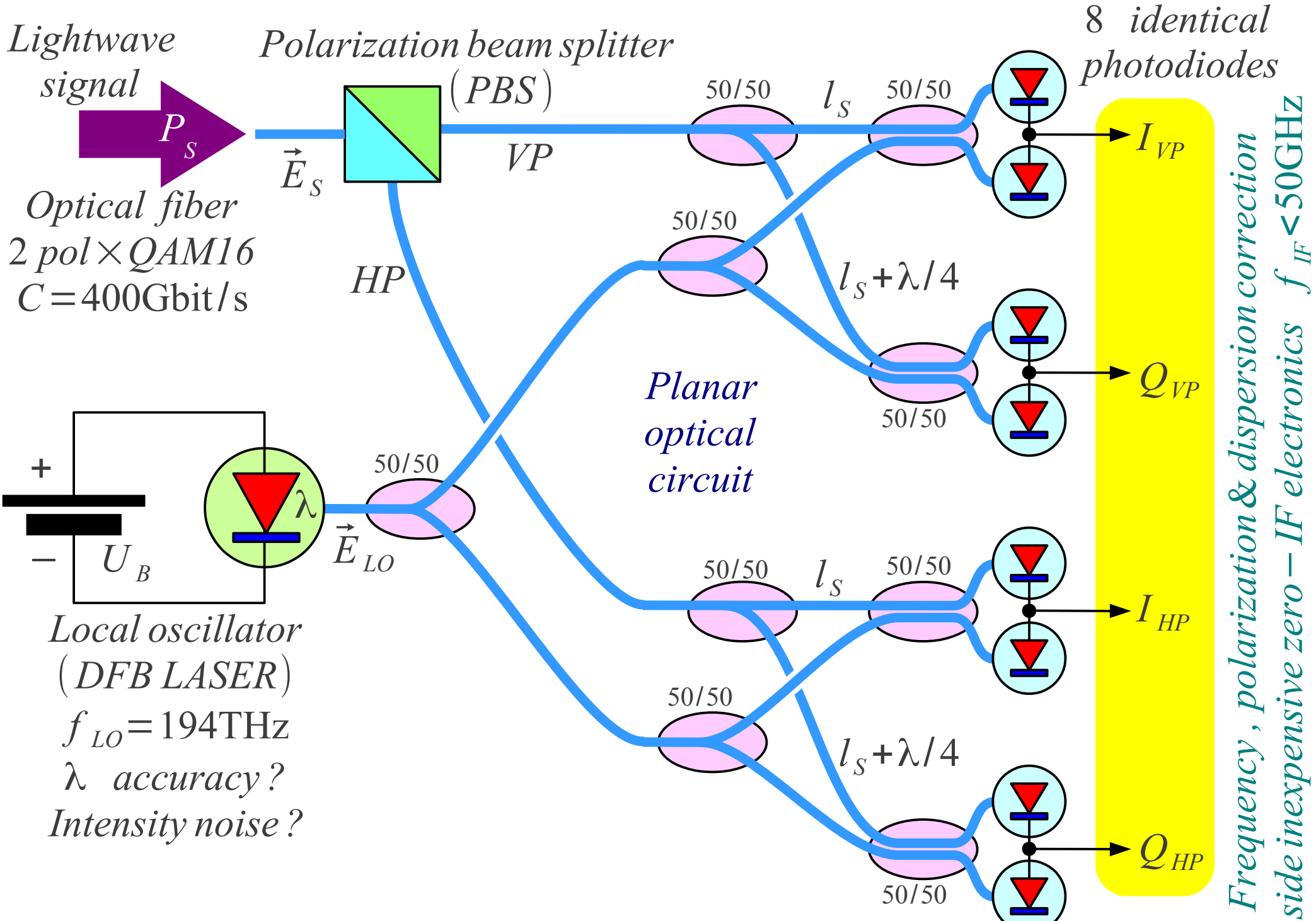
Frequency correction
 $\Delta f = f_{TX} - f_{RX} \neq 0$
 $\Delta f \ll B$

Phasor rotation

Zero-IF QAM receiver



Zero – IF receiver AD8347



*Frequency, polarization & dispersion correction
 inside inexpensive zero-IF electronics $f_{IF} < 50 \text{ GHz}$*

Dual – polarization (MIMO) lightwave receiver